

Original Article

Atom Probe Study of the Miscibility Gap in CuNi Thin Films and Microstructure Development

Rüya Duran*, Patrick Stender, Sebastian Manuel Eich and Guido Schmitz

Institute for Materials Science, Chair of Materials Physics, University of Stuttgart, Heisenbergstr. 3, 70569 Stuttgart, Germany

Abstract

The unclear miscibility of CuNi alloys was investigated with atom probe tomography (APT). Multilayered thin film samples were prepared by ion beam sputtering (IBS) and focused ion beam (FIB) shaping. Long-term isothermal annealing treatments in a UHV furnace were conducted at temperatures of 573, 623, and 673 K to investigate the mixing process. The effective interdiffusion coefficient of the nanocrystalline microstructure (including defect diffusion) was determined to be $D_{\text{eff}} = 1.86 \times 10^{-10} \text{ m}^2/\text{s} \times \exp(-164 \text{ kJ/mol}/RT)$ by fitting periodic composition profiles through a Fourier series. In nonequilibrium states, microstructural defects like grain boundaries and precipitates were observed. While at the two higher temperatures total mixing is observed, a clear experimental evidence is found for a miscibility gap at 573 K with the boundary concentrations of 26 and 66 at%. These two compositions are used in a subregular solution model to reconstruct the phase miscibility gap. So, the critical temperature T_C of the miscibility gap is found to be 608 K at a concentration of 45 at% Ni.

Key words: CuNi alloys, interdiffusion, miscibility gap, thin films

(Received 31 March 2021; revised 1 September 2021; accepted 4 October 2021)

Introduction

CuNi alloys are well-known materials in industry and therefore well investigated. Because of their high corrosion resistance, low macrofouling rates, and good fabricability, they are a good candidate for marine applications like naval condensers and piping. Furthermore, their ductility at low temperatures makes them interesting for components in cryogenic processing and storage compounds (CDA, 2020). CuNi nanoparticles are interesting for their catalytic use in carbon oxide reduction and for the growth of graphene mono- and bilayers (Panizon et al., 2015).

Regarding the phase diagram, however, a miscibility gap at temperatures below 773 K is controversially discussed. The determination of phase boundaries is not an easy task since the diffusivity is very slow at the considered temperatures and phase equilibrium can only be reached with extremely long annealing times (Johnson et al., 1986). Nevertheless, some attempts were made to clarify this issue by indirect experimental measurements and by computational methods which all support the phase separation tendency and the existence of a miscibility gap (Vrijen & Radelaar, 1978; Tomiska & Neckel, 1984; Srikanth & Jacob, 1989; Asta & Foiles, 1996). The reports, however, show large discrepancies with respect to critical temperature T_C and the exact position of the binodal line. To overcome this, direct experimental analysis of the phase boundary composition must be realized. The main difficulties are achieving thermodynamic equilibrium in

reasonable times and using high-resolution composition sensitive measurements.

In this work, the annealing times were reduced by using thin films of just a few nanometers to shorten the necessary diffusion length. The statistical significance is increased by using multilayered diffusion couples with 10 or 20 layers of each. To make sure to be in thermodynamic equilibrium within the selected annealing times, an effective interdiffusion coefficient D_{eff} was determined, which describes the diffusion in both directions, Cu into Ni and Ni into Cu, and includes all kinds of defect transport of the nanocrystalline microstructure, like grain boundary- and dislocation diffusion.

Since grain boundary wetting or interface roughness could be misinterpreted as interdiffusion when using depth profiling with poor lateral resolution, microscopic analysis by atom probe tomography (APT) was performed to characterize the thin film model system. This technique is particularly qualified for its outstanding resolution in the nanometer range and chemical analysis at the same time. Additionally, with the three-dimensional reconstruction, microstructure development can be investigated, which is of great importance here, since some works indicate that Ni-rich and Cu-rich clusters are possible (Gupta et al., 1964; Pawel & Stansbury, 1965; Mozer et al., 1968; Vrijen & Radelaar, 1978; Wagner et al., 1982). Similar APT experiments on multilayered thin films were already carried out in works of Stender et al. (2011) to investigate thermal stability of GMR sensors (Fe/Cr) or analyzing spinodal decomposition in TiAlN/CrN (Povstugar et al., 2013).

Materials and Methods

Suitable samples were prepared by electropolishing a coarse-grained W-wire of 75 μm diameter in a 1 M NaOH electrolyte

*Corresponding author: Rüya Duran, E-mail: rueya.duran@mp.imw.uni-stuttgart.de
Cite this article: Duran R, Stender P, Eich SM, Schmitz G (2022) Atom Probe Study of the Miscibility Gap in CuNi Thin Films and Microstructure Development. *Microsc Microanal* 28, 1359–1369. doi:10.1017/S1431927621012988

solution using a graphite counter electrode to receive needle-shaped tips with a nanometer-sized apex diameter. The tips were further shaped using focused ion beam (FIB) to cut a planar end surface of around $2\ \mu\text{m}$ in diameter (Stender et al., 2011).

On these posts, CuNi multilayers were coated using a custom-built ion beam sputtering (IBS) chamber. The multilayers consist of 10 or 20 layers of each material and a cap of pure Ni to protect the samples against oxidation. As layer materials, pure Cu, and alloyed Ni with 30 at% Cu were used. According to the literature, diffusion of Cu into Ni and *vice versa* show a huge difference [$D_{\text{Ni in Cu}} = 1.80 \times 10^{-21}\ \text{m}^2/\text{s}$ and $D_{\text{Cu in Ni}} = 3.32 \times 10^{-24}\ \text{m}^2/\text{s}$ for $T = 623\ \text{K}$, according to Johnson et al. (1986)]. By pre-alloying the Ni layers, the slow diffusivity of Cu into Ni is partly compensated to reduce the contrast in diffusivities and thus to reach equilibrium in experimentally achievable times (Thomas & Ernest Birchenall, 1952; Arnould & Hild, 2002; Wierzbka & Skibiński, 2016). The layer thicknesses were chosen to achieve an average concentration of 50 at% for each component, that is, 3 nm of Cu and 8 nm of $\text{Ni}_{0.7}\text{Cu}_{0.3}$ (Fig. 1a). To calibrate the thickness monitor of the sputter device, a TEM image from multilayers with 10 nm single layer thickness was taken. For that, a SiO_2 plate has been coated first with one layer CuNi, 25 nm in thickness as a buffer layer, then 10 bilayers of $(\text{Cu}_{10\text{nm}}/\text{Ni}_{10\text{nm}})$. To protect the layers during FIB milling, an additional 500 nm Cr layer

was sputtered. Finally, a lamella of this sample was cut through the standard FIB lift-out process. In Figures 1b and 1c, typical results of the produced microstructure are shown. Although the two metals show nearly no material contrast, the layers can be partly distinguished from the structural interfaces. Layers are planar and in good agreement with the aimed thicknesses. In Figure 1c, a low magnification image is shown as an overview. The colored regions show individual grains determined with dark-field imaging. They have columnar morphology with a lateral diameter of around 25 nm and spread across multiple layers indicating coherent interfaces. Since no chemical contrast is observed, an EDX mapping is recorded with a spot size of 4 nm, as shown in the inset of Figure 1c. Here, the alternating Cu (pink) and Ni (yellow) layers are clearly visible.

The layer systems on W posts were annealed in a UHV furnace with a residual pressure of $<1 \times 10^{-7}$ mbar. The annealing treatments were performed at 573, 623, and 673 K. For each temperature, different annealing durations were carried out, as summarized in Table 1.

After annealing, the samples were sharpened by annular milling (Prosa & Larson, 2017) and measured by a custom-built, laser-assisted APT with a pulsing rate of 200 kHz and a pulse energy of around 150 nJ at a base temperature of 60 K (Schlesiger et al., 2010). Cu and Ni are detected mainly in the

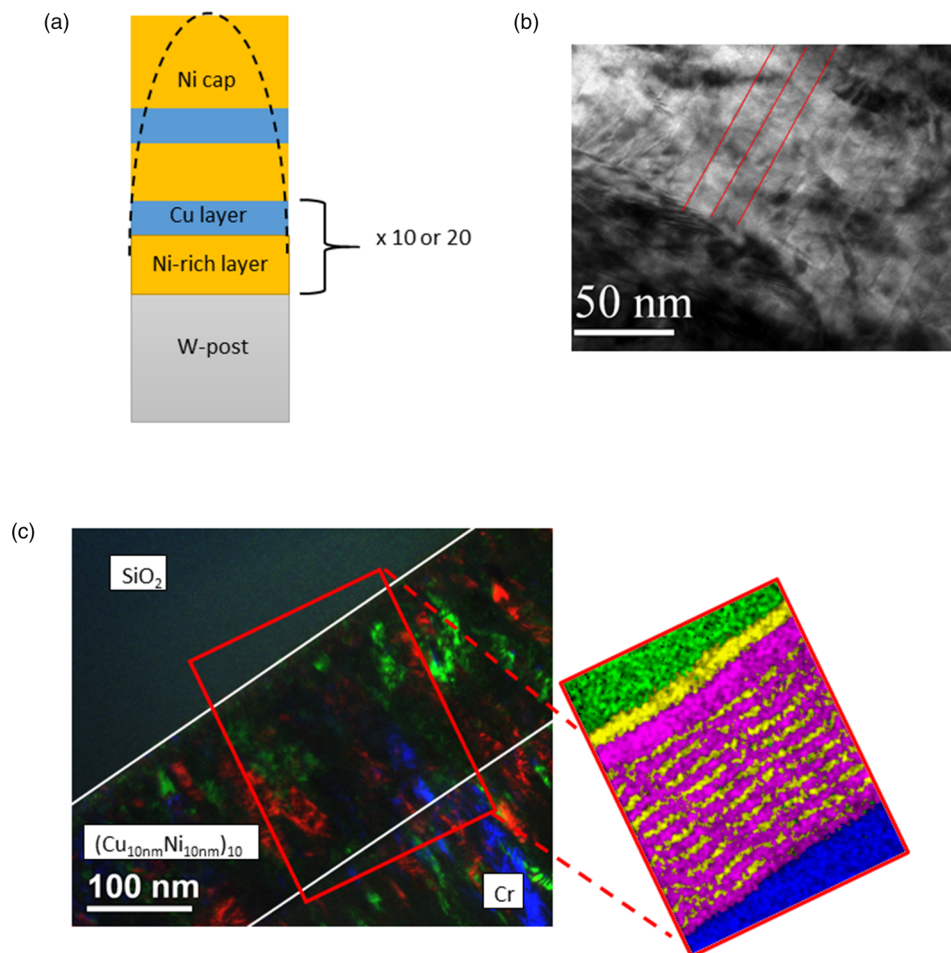


Fig. 1. (a) Schematic illustration of the sample tip. (b) Cross-section TEM image of the multilayer showing that the correct layer thicknesses of around 10 nm per layer has been achieved. (c) Colored overlay of different dark-field images of the same lamella. The colored regions mark grains, which obviously spread through the whole layer system. The chemical layer structure is proven by EDX mapping as shown on the right-hand side.

Table 1. Used annealing times and temperatures.

<i>T</i> (K)	<i>t</i> (d)					
673	1	2.5	4.5	7	11	14
623	7	14				
623*	7	16	30	44	60	
573	88	214	458			

623* has different starting concentrations of $c_2 = 0.7$ and $c_1 = 0.44$.

single charged state with no overlapping mass peaks (see Fig. 2 for an exemplary mass spectrum and Supplementary material for exact peak identification). For the volume reconstruction, the protocol from Bas et al. (1995), which relies on the point projection model, and a geometrical algorithm to determine the tip radius according to Jeske & Schmitz (2001) were used. To calibrate the reconstruction, the lattice plane distances in Cu and Ni layers were adjusted to their theoretical values.

Results

The suitability of the procedure was tested first. To make sure that the layers are created as planned and their concentrations can be measured, an as-prepared sample is analyzed. The volume reconstruction of the tip and a 1D composition profile from a small probing cylinder are shown in Figure 3. The different layers are nearly straight and can be distinguished easily. The reconstruction also shows that the thin Cu layers become narrower at the outside and thicker in the middle. This effect is due to reconstruction artifacts caused by the lower evaporation field of Cu (30 V/nm) in comparison to Ni (35 V/nm). Quantitative analysis is made by

1D composition profiles (Fig. 3b) using a rectangular box perpendicular orientated to the interfaces with a probing volume of $10 \times 10 \times 80 \text{ nm}^3$. Several box sizes and tip regions were tested to find the profile with the best resolution. The Cu compositions of the layers are $(30 \pm 1.4) \text{ at\%}$ and 100 at\% and the layer thicknesses are in accordance with the desired sputtered size. Maximum thickness fluctuations of around 2 nm occur, either caused by sputtering errors or by reconstruction artifacts. Nevertheless, this layer roughness does not affect the equilibrium composition and is therefore of minor interest here.

Microstructural Development

During annealing for different durations, diffusive transport changes the layer structure of the samples until it is fully homogenized or the compositions of heterogeneous phases match the solubility limits. If the annealing time is not sufficient to reach equilibrium, intermediate states will be formed. In Figure 4, tip reconstructions of annealed samples at 673 K for 2.5 d (Fig. 4c) and 4.5 d (Figs. 4a, 4b, 4d) with typical observed microstructures are shown. In Figure 4a, the layer structure is still intact, however, three grain boundaries are visible (red arrows), differing in their composition (60 at% Cu) by segregation from the layers, while the surrounding layer structure is eliminated to an average concentration of around 35 at% Cu. Because of their defective structure, grain boundaries are fast diffusion paths to reach the local equilibrium faster or to provide heterogeneous nucleation sites. During the mixing process, composition fluctuations including precipitate-like volumes of increased concentration will occur as shown in Figure 4b (regions are framed by red dashed line) with concentrations of 29 at% (Ni-rich) and 73 at% of Cu. Often an asymmetric situation is observed where on one side of

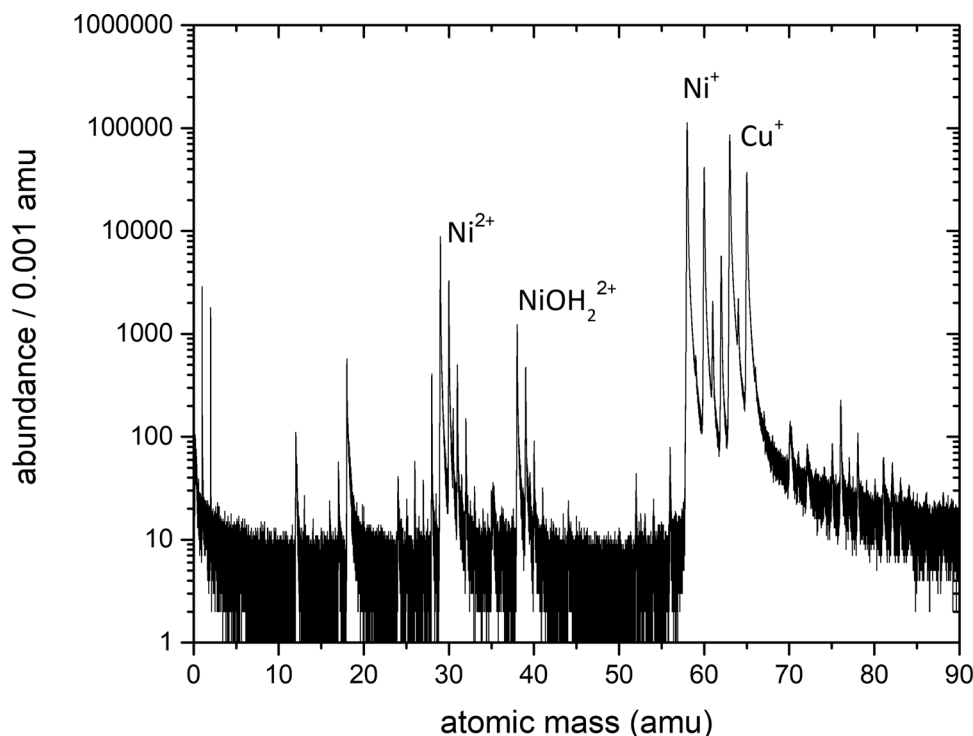


Fig. 2. Exemplary mass spectrum from an atom probe analysis of a sample annealed at 673 K for 2.5 d. The exact peak identification can be found in the Supplementary material.

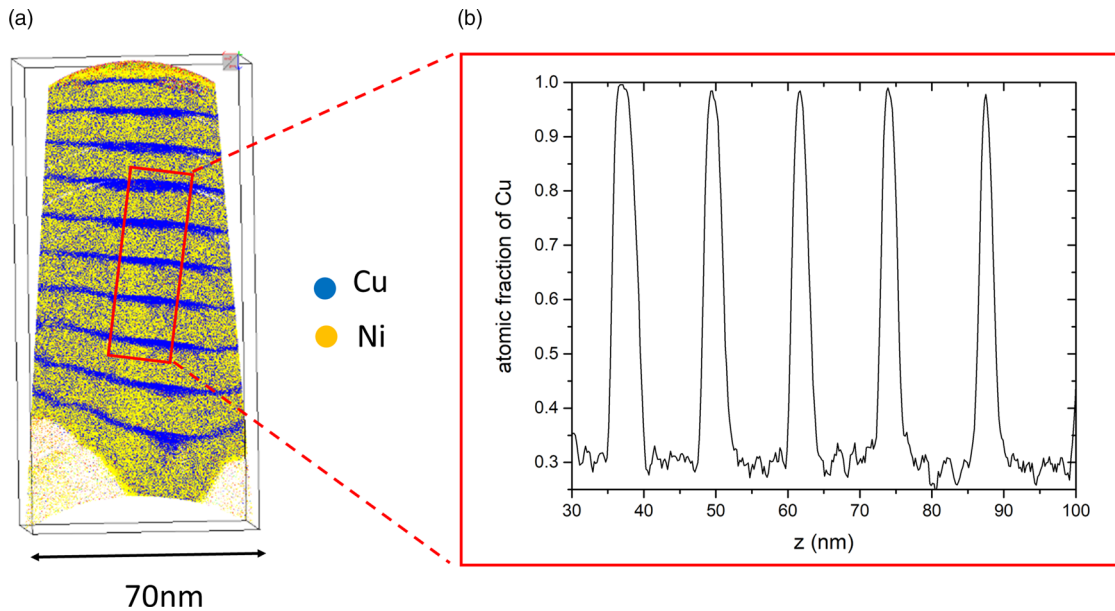


Fig. 3. (a) Cross-section of an as-prepared sample (the low density “triangles” at the bottom are due to the strong contrast of evaporation threshold between Ni and tungsten) and (b) its concentration profile for Cu along the tip axis.

the grain boundary still the layer system is intact while on the other side full mixing is observed ($c_{\text{Cu}} = 48$ at%, Fig. 4c). This geometrical situation indicates mixing by diffusion induced grain boundary migration (DIGM) as suggested for very low temperatures (King, 1987). Finally, the whole specimen appears to be completely mixed (Fig. 4d).

An interesting point is that the intermediate states show pronounced variation although annealing time and temperature were kept almost constant. The reason is, that in the kinetic regime, the microstructure is crucial. Since grain boundaries control the speed of mixing, the more grain boundary area the tip has, the more pronounced is the mixing.

Diffusion Controlled Intermixing

To define the limits of miscibility, the determination of the concentration maxima is insufficient. Especially the narrow Cu layers have probably contributions from the interfaces, which reduces the real concentration. A better approach is to consider the composition profile as a whole and to describe its behavior analytically. In case of diffusion-controlled temperature regimes, this is done by considering the experimental profiles as diffusion profiles and to investigate the samples by their temporal development. Knowing the starting parameters, like layer concentration at $t = 0$ and the annealing time, the profiles can be fitted and some additional parameters like diffusion coefficient and layer concentrations can be determined. Note that in a diffusion-controlled system the diffusion coefficient at different times but for the same temperature is the same and just the layer concentrations change with time.

For an immiscible system, however, the diffusion coefficients will vary with time, since the amplitude of the concentration profile is not changing anymore.

Therefore, composition profiles as shown in Figure 5a are analyzed for different annealing times. To extract these profiles, analysis boxes were placed at regions of the reconstruction where the layering was still visible. The boxes with cross sections of $10 \times$

10 nm and length up to 80 nm were then oriented perpendicular to the interfaces and a composition profile was generated.

Due to the periodic nature (Fig. 5a, top) of the layer stack, the time evolution of the composition profile is described by a Fourier series as follows:

$$c(z, t) = \bar{c} + \sum_{n=1}^{\infty} e^{-(2\pi n/\delta)^2 Dt} a_n \cos\left(\frac{2\pi n}{\delta}(z - z_0)\right). \quad (1)$$

The Fourier coefficients a_n are obtained by integrating over the full period $\delta = \delta_1 + \delta_2$:

$$a_n = \frac{2(c_1 - c_2)}{\pi n} \sin\left(\frac{\pi n \delta_1}{\delta}\right) = \frac{2(c_1 - c_2)}{\pi n} \sin\left(\frac{\pi n (\bar{c} - c_1)}{(c_1 - c_2)}\right), \quad (2)$$

where \bar{c} is the mean concentration, c_1 and c_2 are the initial layer concentrations, and z_0 is the spatial offset. The last identity at the right-hand side holds due to conservation of matter.

Using this equation, experimental concentration profiles for different annealing times and temperatures are fitted. With the knowledge of annealing time t and the initial layer concentration c_1 and c_2 , equation (1) can be used to obtain the diffusion coefficient D , the mean concentration \bar{c} , and the combined layer thickness δ (and offset z_0).

If the concentration in the layers evolve in time in accordance to equation (1) with a constant diffusion coefficient, the process is diffusion controlled and the system will mix completely at this temperature.

The temporal evolution of the mixing can be clearly derived from the composition profiles shown in Figure 5 for 673 K (Fig. 5a) and 623 K (Fig. 5b). The images show the experimental profiles (black crosses) and the corresponding fit (red line) with equation (1). In general, the experimental data are in good agreement, remaining differences are well explained by statistical fluctuation and possibly also some influence of reconstruction artifacts stemming from the different evaporation thresholds.

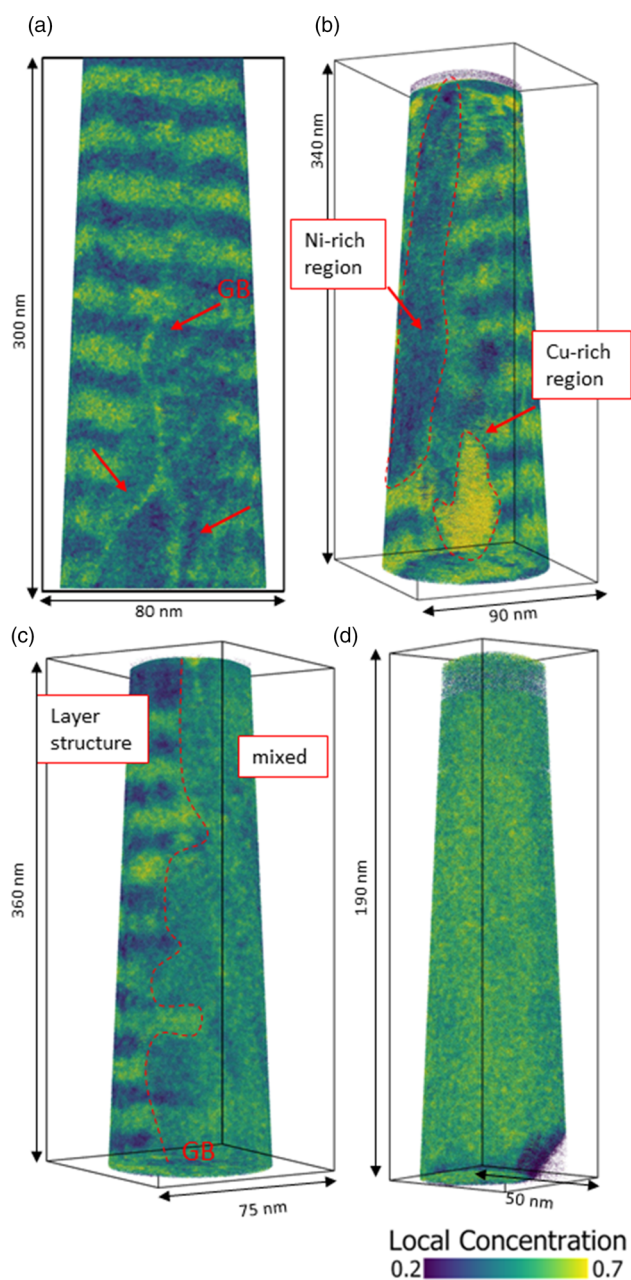


Fig. 4. Local Cu concentration plots of tips annealed at 673 K. Microstructural development of mixing shown at different states. In (a), mixing starts in grain boundaries of a sample annealed for 4.5 d. (b) Nucleation and growth cause composition fluctuations in bulk (annealed for 2.5 d). (c) Diffusion induced grain boundary migration in a sample annealed for 4.5 d. And (d) total mixing of a sample annealed for 4.5 d.

The latter deviations will diminish with the annealing when the samples become chemically more homogeneous. At both temperatures, the diffusion coefficients determined by fitting remain almost constant in the course of annealing.

With increasing annealing time, the profile amplitudes are damped exponentially with time toward the average concentration (blue line). In comparison to the as-prepared state (0 d) the Cu concentration at the Ni-side (minima) of the 2.5 d and 16 d annealed samples shift only slightly (around 4%) to higher Cu concentration, whereas, on the Cu side, a large step to lower concentrations is observed. This indicates the asymmetry in the diffusivities, which is due to the concentration dependence of the

diffusion coefficient. For 673 K, the profile reaches the average concentration after 14 d. Although some noise is still visible, the general trend, clearly indicates that the system is miscible at this temperature.

At 623 K, even after 60 d, a sinusoidal periodicity with 5 at% difference is still visible. However, the concentration amplitudes are continuously decreasing according to the diffusional description. Also, no plateaus of composition are formed which would be the case for phase separation. Assuming that full mixing is just not reached because of too short annealing times, the time necessary to reach phase equilibrium (less than 1 at% remaining amplitude) was determined using D from Figure 6a. It is found that at least 77 d were necessary. So, we can conclude that the system is fully miscible at this temperature.

Since it is clarified that the profiles are diffusion controlled, a diffusion coefficient is determined out of the data. This knowledge is important to determine the annealing times for reaching thermodynamic equilibrium. Although several investigations were performed regarding this topic (Matano, 1932; Anand et al., 1965; Helfmeier & Feller-Kniepmeier, 1970; Johnson et al., 1986), the resulting diffusion coefficients D exhibit a wide scattering range depending on the material structure and the used technique, in particular when extrapolated to the required low temperatures.

Therefore, we determined an effective interdiffusion coefficient D_{eff} valid for the nanocrystalline microstructure of this study, which is directly received from the isothermal annealing sequences by fitting with equation (1). As can be seen in equation (1), the evaluated diffusion coefficient has a quadratic dependency on the thickness. However, since the variation of layer thickness from sample to sample is determined in the fitting process, these variations are correctly treated to determine a reliable diffusion coefficient.

The results for D_{eff} of all profiles (can be found in the Supplementary material) are plotted against the annealing time in Figure 6a. At 623 K (black diamonds), the diffusion coefficients are lower compared with 673 K (blue triangles). Although the diffusion coefficient is concentration dependent, and with time, the concentration in the layers change, the values do not show a trend with the duration of annealing. This means that a concentration dependency of D is not seen here, probably because the average concentration is reached quite fast and D corresponds closely to the concentration of 50 at%.

The coefficients of 54 profiles from 623 K and 45 profiles from 673 K were averaged and plot into an Arrhenius diagram for comparison (Fig. 6b):

The derived characteristic parameters are: $D_0 = 1.86 \times 10^{-10} \text{ m}^2/\text{s}$ and $H = 164 \text{ kJ/mol}$. In the same figure, reported literature data for chemical diffusion of Cu into Ni are shown. The characteristic parameters are presented in Table 2. Although the present study investigated the interdiffusion in a nanocrystalline microstructure (averaged on the full concentration range and possible further defect contribution), they are comparable with the diffusion of pure Cu into Ni polycrystals. The reason is that diffusion in Ni is thousand times slower [see Johnson et al. (1986)] than diffusivity in Cu. This means that volume diffusion of Cu in Ni is the rate-determining process.

Determination of Phase Boundaries

Similar to Figure 5, the composition profiles at 573 K are investigated as shown in Figure 7. In comparison to the higher

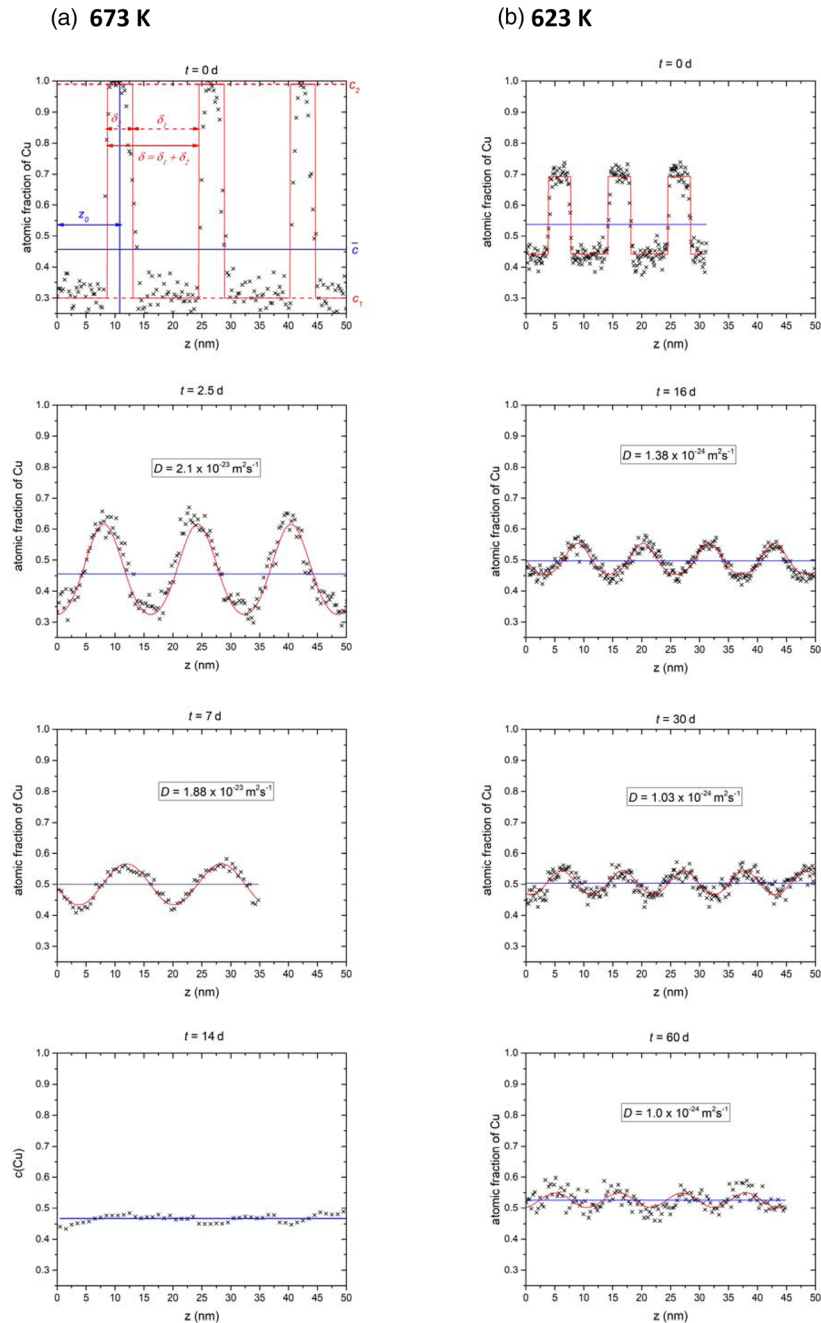


Fig. 5. Exemplary composition profiles for 673 K (**a**) and 623 K (**b**), black crosses) at different annealing times together with the fit (red line) according to equation (1) and the average concentration (blue line).

temperatures, a significant difference in the mixing tendency is observed. A merging of the concentrations appears only after the first annealing time (88 d). But during longer annealing, the concentrations stay practically constant with boundary concentrations at 34.3 and 74.0 at% Cu.

These profiles now represent two phases separated by an interface. Therefore, for quantitative evaluation, the composition profiles across the interface are modeled through sigmoids according to the Cahn–Hilliard approach (Cahn & Hilliard, 1958). Because we have periodic profiles and each period consist of two interfaces (Fig. 7), two sigmoids are required to describe

a full period $h_i(z)$:

$$h_i(z) = \frac{1}{\exp(-4(z - (z_{0,\alpha} + i\delta))/w) + 1} - \frac{1}{\exp(-4(z - (z_{0,\beta} + i\delta))/w) + 1}, \quad (3)$$

where w is a measure of the interface width according to Cahn, δ is the period as described above, and $z_{0,\alpha}$ and $z_{0,\beta}$ are the

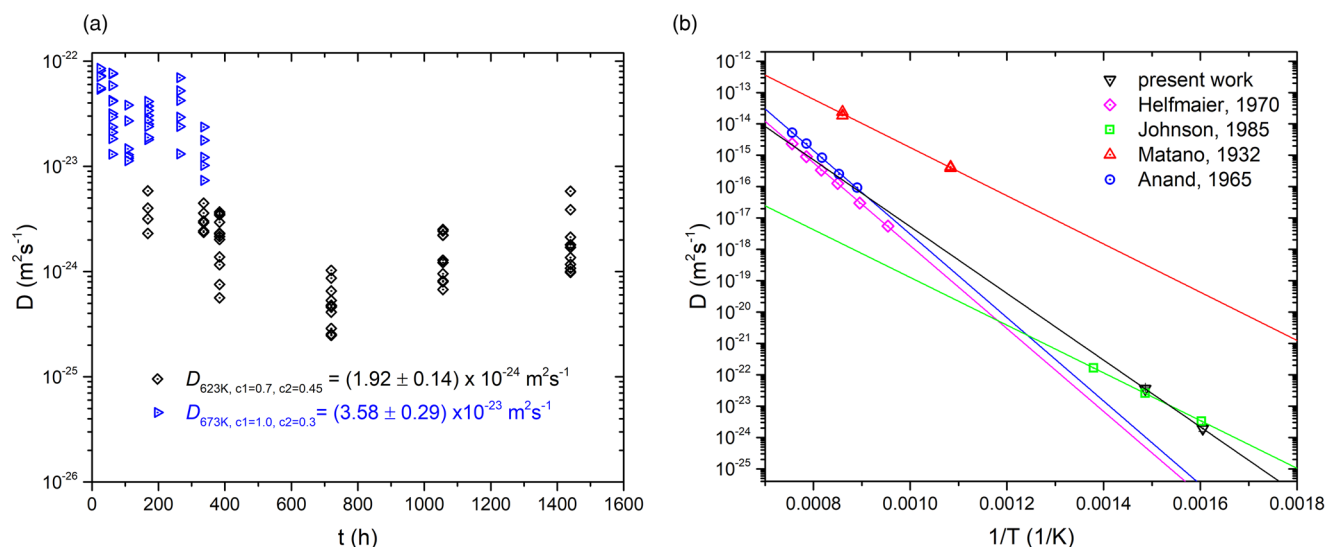


Fig. 6. (a) Diffusion coefficients D of all composition profiles measured in the present work. (b) Arrhenius plots of diffusion data of the present work in comparison to the literature. Helfmaier, Anand, and Matano studied mixing of a Cu thin films into polycrystalline Ni, whereas Johnson et al. investigated interdiffusion of Cu/Ni thin film couples similar as in this study.

Table 2. Comparison of diffusion data found in the literature for diffusion of Cu in Ni with the effective diffusion coefficients D_{eff} determined in this study.

	D_0 (m^2/s)	H (kJ/mol)	Sample preparation	Technique
Present work	1.86×10^{-10}	164	Interdiffusion in thin film couple	APT
Helfmaier	2.7×10^{-5}	255.3	Lattice diffusion from thin film	Microprobe analyzer
Johnson	5.2×10^{-12}	145.7	Interdiffusion in thin film couple	Auger Depth Profiling
Anand	7.24×10^{-5}	255.2	Lattice diffusion with Cu tracer	Residual activity
Matano	1.1×10^{-7}	148.5	Lattice diffusion from thin film	X-ray studies

position of the interfaces. The full composition is given simply by superposition:

$$c(z) = c_2 + (c_2 - c_1) \sum_{i=0}^{n-1} h_i(z). \quad (4)$$

With n as the number of periods and c_1 and c_2 as the compositions of the equilibrium phases.

In Figure 7, the fit is shown as a red line. The plateau concentrations (= equilibrium compositions) are marked with green dashed lines. Note that the received concentrations are slightly above the peak maxima of the fit. This is due to the narrow layer thicknesses of the Cu-rich layers which are so small that the plateau is even not reached. The plateau concentrations found for all samples are listed in the Supplementary material.

To demonstrate that really a phase separation occurred, the annealed profiles were also modeled for the diffusion-controlled case (using D from the extrapolated Arrhenius plot above). They are shown in the plots as dashed blue lines. At $t = 88$ d, the diffusion profile lies nearly exact on the experimental curve, indicating that this short annealing time is still diffusion-controlled. By increasing t to 214 d, a deviation of more than 10 at% at the peak maxima to the experimental curves are seen, whereas the concentration plateaus at the bottom are still fitting well. For 458 d, however, the concentration of the diffusion-

controlled profile show huge discrepancy to the experimental curve and they would be way closer to the overall concentration and thus, clearly a miscibility gap is evidenced.

The observed phase boundaries clearly localize the critical temperature between 573 and 623 K. By calculating the miscibility gap from this data, T_C can be determined more precisely. For that a Redlich–Kister parametrization of the Gibbs energy (Redlich & Kister, 1948) is used according to:

$$g(c, T) = cg^{(2)}(T) + (1 - c)g^{(1)}(T) + k_B T (\ln c + (1 - c) \ln (1 - c)) + c(1 - c) \sum_{i=0}^1 L_i (2c - 1), \quad (5)$$

where the first term is the weighted average of the pure components (which is actually irrelevant for the calculation of the phase boundary), the second term is the configurational entropy, and the third term describes the deviation from ideal behavior (subregular solution).

With the free coefficients L_i and c as the Ni concentration.

Using equation (5) and the double tangent method, the values for L_0 and L_1 were adapted such that the double tangent method reproduces the measured phase boundaries. They are found to be $L_0 = 10.006$ kJ/mol and $L_1 = -0.695$ kJ/mol. The complete

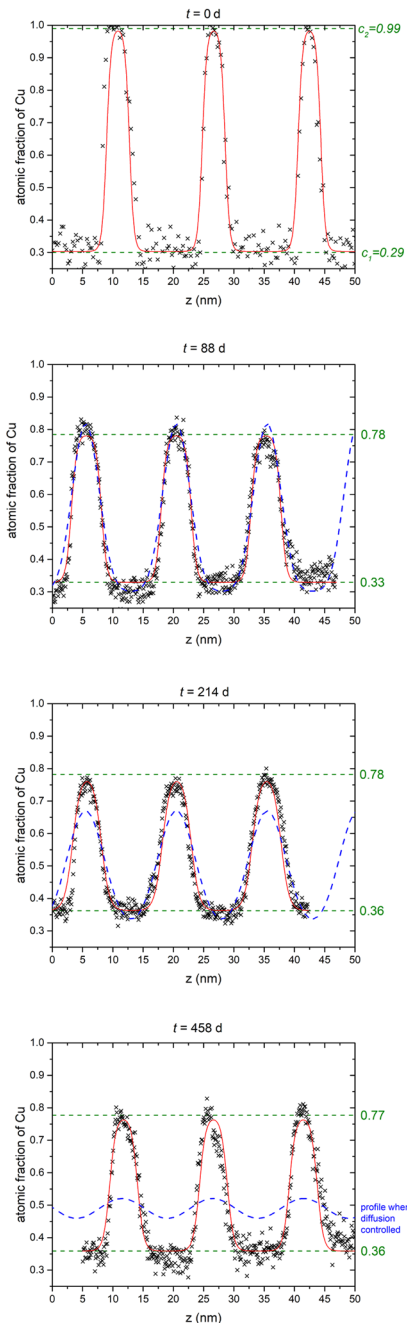


Fig. 7. Exemplary composition profiles for all annealing times of $T = 573$ K (black crosses) with the fit (red line) according to equation (4) and the plateau concentrations (green dashed line). The predicted profile is shown in the $t = 458$ d plot as a dashed blue line.

miscibility gap can be reconstructed with the knowledge of these parameters as shown in Figure 8 as a red line. The same figure contains the experimental phase boundaries (now as Nickel concentration to compare with literature data) and the latest CALPHAD style miscibility gap (Turchanin et al., 2007) data by Turchanin et al. The found parameters of the miscibility gap in this study are 608 K for T_C at a concentration of $c(\text{Ni}) = 0.45$ at % with the phase boundaries of $c(\text{Ni}) = 65.7$ and 26.0 at %.

Considering the critical temperature, the CALPHAD phase diagram is in well agreement to our result with a T_C of 605 K.

However, our experiments cannot confirm the asymmetric shift to higher Ni contents claimed by the CALPHAD approximation. Our miscibility gap is even slightly shifted to the Cu-side.

Discussion

The measured effective diffusion coefficient D_{eff} was compared to literature values for diffusion of Cu in Ni in Figure 5b. Two high temperature measurements were made by Helfmeier and Anand with bulk Ni coated by a thin Cu film. Both studies are in good agreement to each other. However, in comparison to this study, they show a huge discrepancy. On the other hand, our data is nearly identical to previously measured diffusivity by Johnson et al., who used nearly the same temperature range for analysis on deposited Cu/Ni bilayers of 500 nm single layer thicknesses and measured the composition profiles by Scanning Auger Microprobe. The difference to the high temperature reports attributes to the sample microstructure. In the high temperature studies, single crystals or large grained polycrystals were used and so fast diffusion paths like grain boundaries or point and line defects are rare, just lattice diffusion takes place. In the low temperature studies, however, thin films were used, in which, these defects are present in high density and so, the diffusion is controlled largely by short circuit transport. In confirmation we clearly see grain boundaries. The columnar grain boundaries are regions of fast atomic transport and act as nucleation zones for diffusion controlled growth of the new (mixed) phase as shown in Figure 4. During growth, inhomogeneities are observed in bulk and grain boundary migration takes place, leaving a complete mixed phase behind. The mixing seems to be faster for specific orientations (see Fig. 4c). This observation can be explained by the system trying to reduce the nucleation energy by forming a coherent interphase with one of the grains. Consequently, the growth rates are different to both sides of interface (Porter, 2001).

The time-dependent mixing behavior is shown via concentration profiles in Figure 6. The initial concentrations of both layers shift toward the average concentration, whereby the Cu layers make larger steps, which agrees with the faster diffusion of Ni in Cu than *vice versa*. The specimen is totally mixed when the concentration profiles do not oscillate anymore but a plateau at the average concentration has developed.

Comparing the time-dependent measurements of all temperatures as shown in Figure 5, such convergence to the average concentration was just observed for 673 K. At 623 K, the convergence cannot be proven directly, but since all annealing steps can be described by mixing diffusion profiles, it is practically guaranteed that also this temperature lies above miscibility gap. Furthermore, the predicted annealing time of 77 d for reaching equilibrium is not fulfilled in the experiment, where the longest duration of annealing has been 60 d. This can explain the remaining difference of 5 at% between the layer concentrations. By contrast, at 573 K (Fig. 7), stable concentration values were reached after 88 d, although the diffusion model predicts a closer merging. Thus, here the phase boundaries of the miscibility gap have been clearly reached. The phase boundaries are, therefore, localized at 34 and 74 at% for 573 K with a critical temperature at 608 K at a concentration of 45 at% of Ni. These results are compared with the broad spectrum of critical temperatures from the literature (see Table 3). Although most values are made from indirect analysis, they give a rough estimation that T_C lies between 177 and 673 K. The first report on a miscibility gap in CuNi was made by Meijering et al., who analyzed the ternary NiCrCu system and

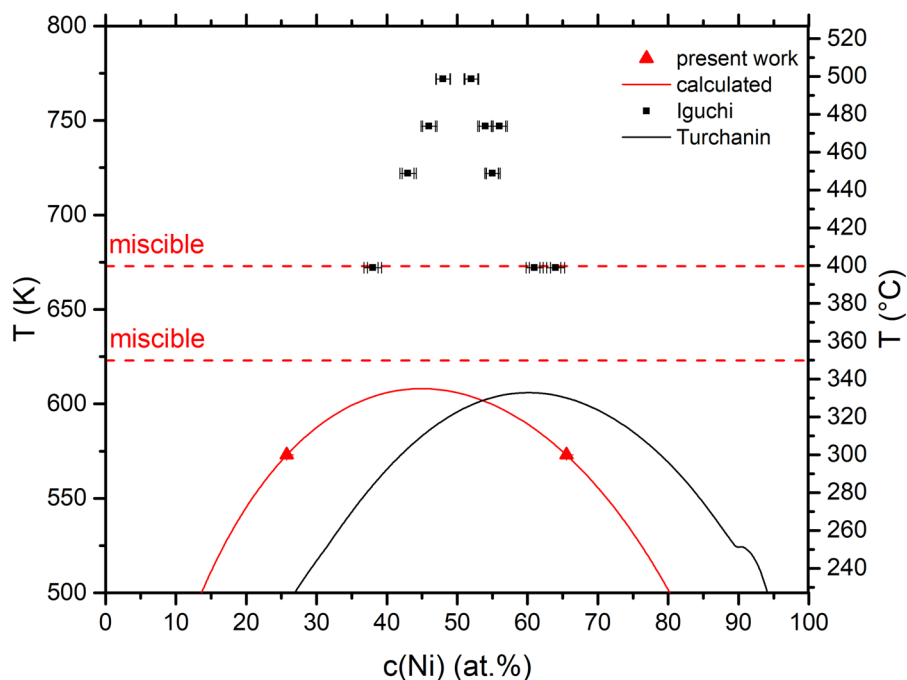


Fig. 8. (a) Measured phase boundaries at 573 K (red triangles) together with the measured miscible temperatures (horizontal, dashed red line) and the calculated miscibility gap (red line). The black line represents the latest CALPHAD miscibility gap and the black squares the one, measured experimentally by Iguchi et al. Note that here, other than in the text above, $c(\text{Ni})$ is used to compare the results to the literature.

Table 3. Literature values for critical temperature T_c and boundary concentration $c(\text{Cu})$ in CuNi alloys.

Reference	Method	T_c (K)	$c(\text{Cu})$ (at%)
Meijering (1957)	Theoretical considerations of ternary phase diagram data	450	
Gupta et al. (1964)	Specific heat measurements	<473	45–55
Pawel and Stansbury (1965)	Specific heat measurements	613–673	25–50
Mozer et al. (1968)	Neutron scattering	506–536	53
Love et al. (1971)	Mössbauer spectroscopy		>60
Ebel (1971)	X-ray diffraction on spinodal decomposition	523	10–90
Lopez et al. (1992)	AP-FIM	473	30
Tsakalagos (1981)	Artificial composition modulation on spinodal decomposition (theoretic)	603	55
Wagner et al. (1982)	Diffuse and small angle neutron diffraction	527, 575	41
Iguchi et al. (2018)	Secondary Neutral Mass Spectroscopy	780	50
Turchanin et al. (2007)	CALPHAD	605	40
Present study	Atom probe tomography	$623 < T_c < 673$	50

found a three phase equilibrium which would just be possible, when CuNi shows phase separation. In fact, they calculated an interaction parameter that leads to a T_c of 450 K, but mentioned that this is just a rough estimate.

Gupta et al. measured the specific heat of CuNi at temperatures below 573 K. They measured phase boundaries with 45–55% Cu content at temperatures lower than 473 K for alloys. However, they did not make any attempt to correct their measurements. Similar calorimetric experiments were made by Pawel et al. for temperatures between 323 and 883 K and alloys of 25 and

50 at% Cu. The T_c that they estimated after corrections is in good agreement to our measured data.

Mozer et al. used a neutron scattering technique on a sample with $c_{\text{Cu}} = 52.5\%$. A tendency of short-range clustering was found between 506 and 536 K, which is below the T_c found in this work. However, Wagner et al. used the same technique and came to a similar result of 527 K like Mozer, but differentiated between a coherent and an incoherent miscibility gap. The T_c of their incoherent gap has been found to be 575 K, which is very similar to our result.

X-ray measurements were made by Ebel et al. at a temperature of 523 K for different alloy concentrations. They measured spinodal decomposition ranging from 10 to 90 at%. Although we have no direct measurements at this temperature, the phase borders of the calculated miscibility gap lie in the same regime.

In Lopez et al., an alloy with 30 at% Cu content was annealed at 573 and 473 K and measured with APT. Out of the determined correlation coefficient, a clear decomposition was observed for 473 K which became weaker for 573 K, indicating that this temperature is closer to the critical temperature.

Tsalakos et al. analyzed a T_C for $c(\text{Cu}) = 55$ at%. They measured multilayer samples of 5 nm single layer thickness with X-ray diffraction and used the “artificial modulation technique” to find out T_C . In this technique, the amplitude of a composition wave is analyzed. The variation of the amplitude with annealing time is proportional to the peak intensity and thus, to the composition. By this, they came to a T_C of 603 K which is in good agreement with our measurements.

By contrast, recently, another new experimental study was undertaken by Iguchi et al. using the “diffusion couple technique” for bi- and trilayer thin films of pure Cu and Ni (30–70 nm) and measuring the composition directly via depth profiling with Secondary Neutral Mass Spectrometry (SNMS; Iguchi et al., 2018). They received a T_C of 780 K at a composition of 50 at% Cu, which is quite above the values reported earlier and not at least motivated us to recheck the result for layer mixing. Furthermore, their suggested shape of the solubility gap does not resemble the typical shape obtained from a (sub)regular solution model. It is in general too narrow. Our new data clearly contradict this proposition.

However, when checking the annealing times of Iguchi et al. with our diffusion model, but considering their sample depths (30 nm each) and concentrations, it is obvious that the studied annealing times of 168 h are by far not sufficient to reach equilibrium at 673 and 723 K, which should be at least 2662 and 362 h. So probably their high T_C and the irregular phase boundaries are a consequence of insufficient annealing.

In the Turchanin *et al.* phase diagram, the proposed T_C (see Fig. 8b) is in good agreement to our result. For this proposition, various experimental investigations on alloy properties (structural, electrical, and magnetic) were taken into account. In comparison to other CALPHAD approaches, Turchanin considered not just mixing enthalpies and activities from the liquid solutions, but also from solid solutions and they considered magnetic effects. Additionally, it is the only calculation, made in a self-consistent description of all data on thermodynamic properties.

While T_C convincingly agrees, a huge discrepancy is seen regarding the phase boundaries between the suggested phase diagram and our experimental data. The Cu-rich phase boundary at 573 K contains around 13 at% more Ni than our results, whereas the Ni-rich phase shows a difference of 10 at%. Especially when considering the Cu-rich side (fast diffusion), the used annealing times in our experiment have to be long enough for reaching equilibrium. This can be seen also from the stable concentration values in dependence of the annealing time (Fig. 7). Only on the Ni-rich side, the slow kinetics may still allow a remaining deviation from equilibrium. Here, further demixing could shift the experimental phase boundary to Turchanin's suggestion. But the significant asymmetric positioning in the composition range appears inconsistent with our experimental findings. Further mixing experiments at temperatures above 573 K and

close to T_C can help clarifying this. However, the predicted annealing time at $T_C = 608$ K is 148 d and thus quite long.

Summary

An approach for direct measurements of phase boundaries of the miscibility gap for slow diffusion couples was introduced. By using thin films of 8 nm thickness and thinner, the diffusion length could be significantly reduced. A further decrease of the annealing time is achieved by using a 30 at% pre-alloyed CuNi layer instead of pure Ni to overcome the slow diffusion on the Ni side. For evaluation, concentration profiles were used and compared to theoretical models. Isothermal annealing treatments were carried out. The results were used to determine first the effective interdiffusion coefficient D_{eff} which is $D_{\text{eff}} = 1.86 \times 10^{-10} \text{ m}^2/\text{s} \times \exp(-164 \text{ kJ/mol}/RT)$. For 573 K, the results clearly do not follow diffusional mixing. This gives clear evidence that these limiting concentrations of $c_1(\text{Cu}) = 74.0$ at% and $c_2(\text{Cu}) = 34.3$ at% represent the real phase boundaries of the miscibility gap. With this, the miscibility gap was calculated using the Redlich–Kister parametrization of the Gibbs energy and the parameters L_0 and L_1 were determined. In comparison to the literature, the results on the critical temperature agree reasonable with the findings from Pawel and Tsakalagos and Turchanin but reject recent experimental studies by Iguchi et al.

Supplementary material. To view supplementary material for this article, please visit <https://doi.org/10.1017/S1431927621012988>.

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