

Long-term effects of an iron heater and Äspö groundwater on smectite clays: Chemical and hydromechanical results from the *in situ* alternative buffer material (ABM) test package 2

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ABSTRACT: Smectite-rich clays are to be used in nuclear repositories for sealing in the radioactive waste. As the radioactive decay produces heat it may affect the chemical, physical and hydromechanical properties of the clay components in the repository. An ‘alternative buffer material’ (ABM) experiment is a Svensk Kärnbränslehantering AB (SKB)-led *in situ* heating test placed in boreholes in the Äspö tunnel (Sweden). The 2nd ABM package was dismantled in April 2013, after 6.5 y of equilibration with Äspö groundwater and 5 y of heating. The objective was to investigate the long-term effects of the iron heater and Äspö groundwater on four of 31 compacted blocks made of MX-80, Deponit CaN and Friedland clays.

Compared to the starting materials, major changes in the exchangeable cation populations were observed. Within horizontal profiles, water-soluble sulfate, Ca, K and Mg increased; poorly crystalline Fe oxide contents decreased; total Mg, Ca and S increased; and a decrease in the amounts of total Na and K away from the host rock towards the heater was observed. At the boundary with the heater, an increase in the total Fe content, decreases in total Si and Al contents, precipitation of gypsum and anhydrite, dissolution of cristobalite and feldspars, and indications of the formation of trioctahedral clay minerals were observed. A decrease in swelling pressure for the Friedland clay (in drill-cored samples) was recorded which was recovered after grinding and recompaction. No effects of hydraulic conductivity were found, after 6.5 y of reaction time, in the subsurface of any of materials studied.

KEYWORDS: chemistry, mineralogy, nuclear waste disposal, *in situ* tests, Fe–bentonite interaction, swelling pressure.

The chemistry and physical properties of clay materials used in nuclear waste repository buffer systems are modified through interactions with surrounding groundwater, by the degradation products of structural components consisting of Fe, Cu or cement, or by heat produced by the fuel canister. In the alternative buffer

material (ABM) experiment, six packages (ABM1–6) containing steel heaters surrounded by stacks of compacted bentonite rings of various clay materials were placed in boreholes in the Äspö hard-rock laboratory at a depth of ~450 m. The package surfaces were sealed with layers of concrete. To increase the water distribution along the test package, the slot between the buffer package and the rock was filled with sand (Eng *et al.*, 2007). Heating of ABM1 started simultaneously with saturation whereas heating of the

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ABM2 package was started only after the bentonite was fully saturated.

The 1st ABM package was dismantled in 2009 after 2.5 y of heating, of which 1.5 y was at the maximum temperature (130°C). The chemical changes found included a general change in the exchangeable cation composition (Kumpulainen & Kiviranta, 2011; Svensson *et al.*, 2011; Dohrmann *et al.*, 2013) and accumulation of water-soluble sulfate (Muurinen, 2010; Kumpulainen & Kiviranta, 2011; Svensson *et al.*, 2011) and Mg (Svensson *et al.*, 2011; Kaufhold *et al.*, 2013) in horizontal profiles towards the iron heater. In addition, a decrease in swelling pressure was observed in core-drilled samples in some materials but no difference in hydraulic conductivity was recorded between samples from the field experiment and the corresponding reference materials (Kumpulainen & Kiviranta, 2011; Svensson *et al.*, 2011). In contact with the heater or close to it, Fe accumulated in bentonite (Kumpulainen & Kiviranta, 2011; Svensson *et al.*, 2011). Dissolution of carbonates, the formation of trioctahedral minerals/domains, the precipitation of siderite and anhydrite, and dissolution of clinoptilolite and cristobalite were found only in certain bentonites (Svensson *et al.*, 2011; Kaufhold *et al.*, 2013).

The 2nd ABM package was dismantled in 2013 after equilibrating for ~6.5 y and after 5 y of heating, of which ~3–4 y was at the maximum temperature (130°C). Details of the experimental design and dismantling procedure were presented by Svensk Kärnbränslehantering AB (2014) and Svensson *et al.* (2011). The scope of the present study was to examine long-term changes in the ABM2 samples due to Fe–bentonite interaction and hydrothermal alteration and compare the ABM2 results with the results from the ABM1 package and reference samples. For comparison, the same methods were applied as in the previous studies (Kumpulainen & Kiviranta, 2010, 2011; Muurinen, 2010).

MATERIALS

Upon dismantling of the ABM2 package, some of the blocks were found to be more fragile than in the ABM1 package and thus could not be sampled intact. The blocks selected for the present study, namely block 2 (MX-80), block 4 (Friedland clay), block 5 (Deponit-CaN) and block 6 (MX-80) were located side by side in the lower part of the ABM2 parcel (Fig. 1a). Samples from blocks 4, 5 and 6, were taken for analyses at various distances along the horizontal profiles (B4Fr: 0–3 mm, 3–20 mm, 20–37 mm, 54–74 mm and 89–

94 mm; B5Dep: 0–3 mm, 3–21 mm, 21–31 mm, 44–60 mm and 76–92 mm; B6Mx: 0–4 mm, 4–21 mm, 21–35 mm, 49–63 mm and 77–97 mm) (Fig. 1b). In addition, heater contact samples (B4Fr 0–1 mm, B5Dep 0–1 mm, B6Mx 0–1 mm) for mineralogical analyses were scraped from other pieces of the blocks studied.

Sampling was by means of a knife, band saw, or by core-drilling. Drill-cored samples were used as received for swelling-pressure and hydraulic-conductivity tests (Fig. 1c). Bulk samples were dried at 60°C and crushed in an agate mortar using a pestle. Recompact samples for swelling pressure and hydraulic conductivity measurements that were taken from the same distance from the heater as the core-drilled samples, were crushed gently and recompact to the same density as the corresponding core-drilled samples. Clay fractions were separated from wet, non-ground bulk samples of B6Mx 4–21 mm, B5Dep 3–21 mm, and B4Fr 3–20 mm by suspending the bulk sample in deionized water, adding NaCl salt, followed by centrifugation, and decantation of the clear supernatant. Excess salts were then washed off by repeated addition of deionized water and centrifugation, and finally by dialysis (Spectrapore 3, 3500 MWCO pore size dialysis membrane). Then, the coarse fraction (>0.5 µm) was separated by sedimentation (with the assistance of centrifugation) and the supernatant was removed carefully using a pipette. Salt treatment, washing, and dialysis were repeated twice thereafter for the supernatant. The <0.5 µm fraction was selected in order to remove accessory minerals from clay minerals more efficiently. Some of the Na-converted clay suspension was exchanged to the Mg-form for XRD analysis, and the remainder was dried at 60°C, ground with an oscillating mill to ~10 µm, and analysed for CEC and chemical composition.

METHODS

Chemical composition

Water extraction was performed to obtain information about the composition of solutes and soluble salts in the bentonite. The ground bulk sample was dispersed in deionized water (solid:liquid ratio of 1:100) by mixing with a magnetic stirrer for 24 h. The solids were then separated from the supernatant by centrifugation (1100 rpm, 90 min), and filtration through 0.45 µm and 0.2 µm pore size filters. Part of the supernatant was further filtered through a 0.1 µm pore size filter for inductively coupled plasma-atomic

(determined gravimetrically at 105°C) and were reported as equivalent charges/kg of dry weight.

Bulk chemical compositions and speciation of C and S of the bulk material and of the Na-homioionic <0.5 µm fraction of the bentonite were determined at ACME Analytical Laboratories, Canada. Si, Al, Fe, Mg, Ca, Na, K, Ti, P, Mn, Cr, Ba, Ni, Sr, Zr, Y, Nb and Sc were determined by ICP emission or mass spectroscopy using standard techniques for silicate analysis (LiBO₂/Li₂B₄O fusion followed by nitric-acid digestion). Loss on ignition (LOI) was determined as the difference in weight of the dried (at 105°C) and the ignited sample (at 1000°C). Total carbon and sulfur were determined by evolved gas analysis (EGA) by combustion of the samples in a LECO furnace, equipped with IR detectors. Organic carbon was determined as CO₂ evolved after treatment of a sub-sample with hot 15% HCl. Sulfate was determined on separate samples pre-ignited at 550°C. The concentrations of sulfide-S and inorganic C were estimated by subtracting the concentrations of sulfate-S and organic C from the total concentrations of S and C, respectively. The results from the ABM2 experiment were compared with those in reference samples that have been calculated from Kumpulainen & Kiviranta (2010) by adjusting the adsorbed-water contents. Standard deviation of duplicate analyses of ABM2 samples were 0.09 wt.% for SiO₂, 0.07 wt.% for Al₂O₃ and total-C, 0.02 for Fe₂O₃, 0.01 wt.% for Na₂O and total S, and <0.01 wt.% for MgO, CaO, K₂O, TiO₂, sulfate-S and organic-C.

Citrate-bicarbonate-dithionite extraction (CBD) was used to determine the amount of poorly crystalline Fe oxides in the bulk sample and in the purified clay fraction. 0.5 g of ground material was placed in a centrifuge tube. 20 mL of 0.3 M Na-citrate solution and 2.5 mL of 1 M NaHCO₃ solution were added, the tube was placed in a water bath, heated at 80°C and 0.17 g of Na₂S₂O₄ was added and the mixture was stirred constantly for 1 min with a glass rod and then occasionally for 5 min. Addition of sodium dithionite and mixing were repeated twice, and the mixture was allowed to cool. A mixture of saturated NaCl solution and deionized water was added to induce flocculation, and the suspension was centrifuged. The supernatant was collected and filtered through 0.45 µm pore-size filter. The residue was then washed with saturated NaCl solution and deionized water, followed by centrifugation and filtration. The filtered supernatant solution was diluted to 100 mL with deionized water. Concentrations of dissolved Fe, Si, Al and Mg were determined by ICP-AES analysis at Labtium Oy,

Finland. The results were adjusted against adsorbed water content (determined gravimetrically at 105°C).

MINERALOGICAL METHODS

For mineralogical analyses, the bulk samples were ground in an agate pestle and mortar using acetone. Approximately 10 mg of the ground bulk materials were mixed with acetone on a glass slide and placed in a desiccator that contained saturated Mg(NO₃)₂ solution to achieve standard relative humidity (54% RH at 2°C), for at least 5 days. Subsequently the samples were transferred one by one to a rotating sample holder and scanned from 2 to 70°2θ with a Bruker D8 Advance X-ray diffractometer equipped with a Cu tube and Lynxeye XE detector. The goniometer radius was 280.0 mm. Samples were scanned using a fixed slit, a voltage of 40 kV and current of 40 mA, and a 0.5 s step-time with 0.01°2θ counting step at the Geological Survey of Finland.

The clay mineralogy was determined by X-ray diffraction (XRD) of samples at a distance of ~3–21 mm from the heater, using oriented mounts prepared from purified, Mg-saturated <0.5 µm clay fractions. The filter-membrane peel-off technique was used for preparation of the mounts (Drever, 1973; Moore & Reynolds, 1989). A concentrated suspension was vacuum filtered onto a 0.45 µm pore-size cellulose filter and transferred to a glass slide. Sample mounts were dried in air, kept at least overnight in a desiccator that contained saturated Mg(NO₃)₂ solution, and scanned from 2 to 35°2θ with 0.2 s step-time with 0.02°2θ counting step at the Geological Survey of Finland. Subsequently they were placed in a desiccator containing EG and put into an oven at 60°C for 20 h. The EG-solvated mounts were scanned from 2 to 35°2θ with 0.2 s step-time and 0.02°2θ counting step to identify smectites. Then, mounts were placed in the furnace for 2 h at 550°C, and scanned from 2 to 35°2θ to identify kaolinite.

The bulk mineralogical composition was determined from randomly oriented XRD patterns of bulk samples using a full-profile Rietveld refinement in the *Siroquant* software version 3 that includes a clay package for quantifying clay minerals with unknown crystal structures such as montmorillonite. However, as Friedland clay contains mixed-layer illite-smectite (I-S) which cannot be modeled directly using *Siroquant*, it was treated in the analysis as two separate mineral phases: smectite and illite. The same mineral phases were included in quantifications of all samples of the horizontal profiles as well as the reference samples. After subtraction of the background, refinement was

performed in subsequent stages until no major improvement in pattern fit was achieved. Instrument zero, phase scales, half-widths, unit-cell dimensions, and preferred orientation were refined. Mineralogical composition was validated by comparison of the calculated chemical composition with the observed chemical data. Smectite and illite-mica contents were adjusted assuming that all K (from chemical composition of purified clay fraction) was bound to illite and that the illite-smectite ratio was constant in all samples of the horizontal profile. The smectite structural formula was calculated from the chemical composition of purified <0.5 µm clay fractions for MX-80 and Deponit CaN according to Newman & Brown (1987), after extracting CBD-extractable Fe, and illite content (assuming ideal composition), and taking into account exchangeable cation results. The accessory mineral contents from mineralogical analysis were compared with the calculated mineral contents assuming that all Ti was bound to anatase, all inorganic carbon was bound to calcite (MX-80 and Deponit CaN) or siderite (Friedland clay), all sulfate was bound to gypsum, and that the remaining sulfur was in pyrite.

The decrease in CEC due to Li uptake was performed to identify the charge location in the smectite structure (octahedral vs. tetrahedral). Firstly, to separate the clay, the bulk samples taken ~20–37 mm from the heater were dispersed in 3 M LiCl, stirred for 24 h, washed with deionized water, and <0.5 µm fractions were separated by sedimentation. The clay fractions were treated once with 3 M LiCl solution, and washed with deionized water until incipient dispersion and excess salts were then removed by dialysis (Spectrapore 3, 3500 MWCO pore-size dialysis membrane). Samples were dried at 60°C, ground with an oscillating mill and agate mortar, placed in a porcelain crucible and heated at 250°C for 24 h. After heating, the samples were ground again before CEC determination (see the description for CEC determination above).

Hydromechanical tests

Swelling pressure and hydraulic conductivity were measured first by placing core-drilled samples into fixed-volume swelling-pressure cells, between porous frits, piston and force transducer. Pre-stress loads of ~10% of expected equilibrium swelling pressure were established on each sample prior to saturation. De-aired salt solution (10 g/L NaCl) was used as the saturating solution, which was first allowed to flow slowly through the bottom circuit of the cells, and thereafter through

both the top and bottom circuits of the cells. Axial force due to sample swelling was logged until it was stabilized, and after that hydraulic conductivity measurement was started by increasing the water pressure (using a pressure panel) into one of the cell-bottom circuits to a load pressure of ~50–350 kN, which did not exceed half of the measured swelling pressure in any of the samples. One end of a clear tubing of known diameter was attached to one of the cell-top circuit ports with the other end remaining open to the atmosphere. The volume of fluid permeating through the sample and out of the cell-top circuit was measured as a function of time. Subsequently the saturated sample was removed from the swelling-pressure cell, the dimensions were measured, the water content was determined gravimetrically at 105°C and the bulk density was determined gravimetrically by immersing the sample in paraffin oil. After the density had been determined, neighbouring samples (taken from the same distance as the cored samples) were ground, compressed to the same density, and swelling pressure and hydraulic conductivity measurements were repeated.

RESULTS

Water-soluble ions

Analysis of water-soluble ions showed accumulation of water-soluble sulfate, Ca, Mg and K in horizontal profiles near the heater (Fig. 2). An opposing, decreasing trend towards the heater was recorded for water-soluble chloride contents. In B5Dep and B6Mx profiles, the maximum for water-soluble K, Ca, Mg and SO₄ was found at the heater contact. In the B4Fr profile, the maximum for water-soluble K, Ca, Mg and SO₄ was observed at ~10–30 mm from the heater. In the B6Mx profile, the water-soluble Si and Fe contents increased at the cool end of the profile.

Comparison of water-soluble SO₄²⁻ and Cl⁻ contents in ABM2 samples with the reference samples (Muurinen, 2010; Svensson *et al.*, 2011) showed that the SO₄²⁻ was redistributed in the ABM2 samples compared to the reference samples whereas Cl⁻ contents increased in ABM2 samples compared to the reference samples (Fig. 2).

CBD-extractable Fe, Al, Si and Mg

Citrate-bicarbonate-dithionite-extractable Fe decreased steadily in horizontal profiles B4Fr and B5Dep towards the heater (Fig. 3). In contrast, CBD-extractable Mg increased towards the heater in all the

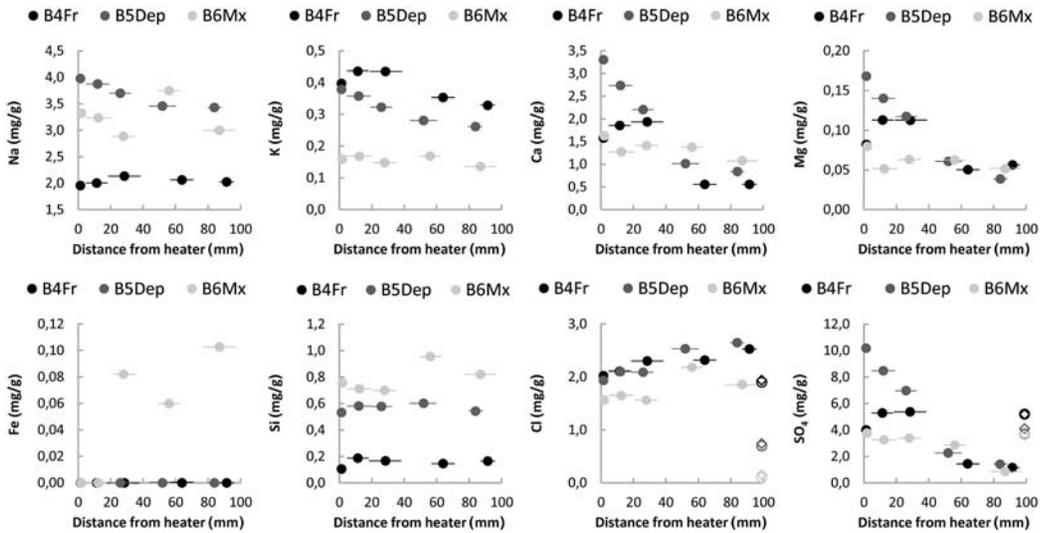


FIG. 2. Aqueous soluble ions as a function of the distance from the heater. Open symbols shown for Cl and SO_4 are reference levels from Muurinen (2010) (circles) and Svensson *et al.* (2011) (diamonds).

materials studied (Fig. 3). In the B4Fr profile, the CBD-extractable Al contents also increased slightly towards the heater. There was also a clear decreasing trend in CBD-extractable Si in B5Dep horizontal profile towards the heater (Fig. 3).

The amount of CBD-extractable Fe_2O_3 and SiO_2 was smaller in ABM2 Friedland clay and Deponit CaN bulk samples than in reference bulk samples reported by Kumpulainen & Kiviranta (2011) and Svensson *et al.* (2011). The amount of CBD-extractable MgO in all ABM2 samples was significantly smaller than the reference samples (Fig. 3).

Exchangeable cations and CEC

In general, exchangeable cation contents, the sum of exchangeable cations and CEC were comparable in all samples of the horizontal profiles, with few exceptions.

The amounts of exchangeable Mg, especially in B6Mx, and exchangeable Ca (and thus also the sum of exchangeable cations) appeared to be slightly higher at or in the vicinity of the heater (Fig. 4). Further, in the B5Dep horizontal profile, the CEC appeared to increase slightly from 0.83 eq/kg at the rock contact to 0.87 eq/kg at the heater contact (Fig. 4).

Comparing the ABM2 results with the reference samples (Kumpulainen & Kiviranta 2010), saturation of exchangeable cation sites had changed dramatically in all ABM2 samples. The changes were similar in all materials: increase in Ca, and decrease in Na, Mg and K. The CEC of ABM2 samples did not change compared to the reference samples. The sum of exchangeable cations in the ABM2 samples was $\sim 0.05\text{--}0.2$ eq/kg smaller than the reference samples in all the materials studied, but it was also (in MX-80 and Deponit CaN) ~ 0.1 eq/kg smaller than the measured CEC.

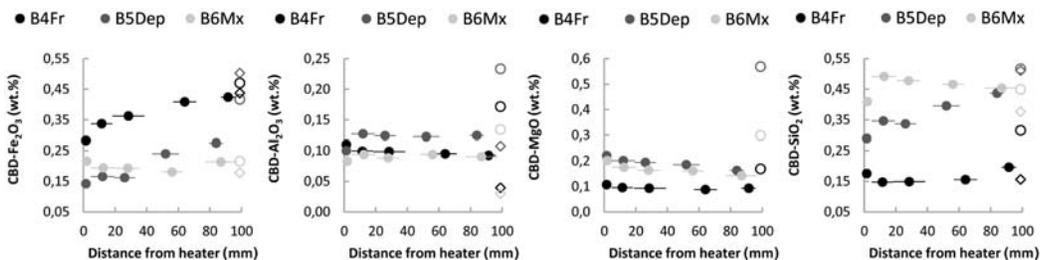


FIG. 3. CBD-extractable Al_2O_3 , Fe_2O_3 , MgO and SiO_2 as a function of the distance from the heater. Open symbols are reference levels from Kumpulainen & Kiviranta (2011) (circles) and Svensson *et al.* (2011) (diamonds).

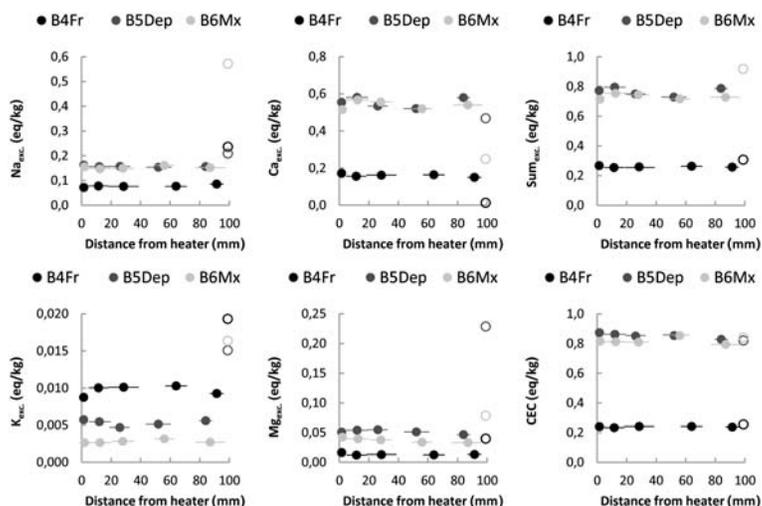


FIG. 4. Exchangeable cations and CEC values (as eq/kg of dry (105°C) mass) as a function of the distance from the heater. Open symbols are reference levels from Kumpulainen & Kiviranta (2011) (circles).

Total chemical compositions

Loss on ignition (LOI) increased in the horizontal profiles in the vicinity of the heater in B6Mx (from 12.4 to 13.5 wt.%) and B5Dep (from 15.3 to 16.0 wt.%), but not in Friedland clay (Fig. 5). Increase in LOI originated from the increase in total C and total S. The increase in inorganic carbon, indicating precipitation of carbonates, was noted in the horizontal profile of B4Fr towards the heater and in the sample in contact with the heater from the B5Dep profile. On the other hand, an increase in organic carbon content explained the increase in total carbon in the B5Dep profile, and in the heater-contact sample of B6Mx (Fig. 5).

All of the materials studied showed a general increasing trend in total S towards the heater. This increase was due to a general increase in sulfate towards the heater in B5Dep (0.51–0.63 wt.%) and B6Mx (0.15–0.26 wt.%). Horizontal profile B4Fr had a sulfate maximum (0.44 wt.%) at a distance of 20–37 mm from the heater, and the B5Dep profile had an apparent sulfidic S maximum at the same distance (Fig. 5).

The Al content decreased in the heater-contact samples in all materials, whereas Si decreased not only in the contact sample but also close to the contact (distance of 3–21 mm). The opposite trend was observed in horizontal profiles for Mg contents, *i.e.* an increasing trend towards the heater. The Ca content also increased slightly in horizontal profiles towards the heater (Fig. 5). The opposite was noted for Na and K contents, which decreased slightly in horizontal profiles

towards the heater. The only exceptions were that in the heater-contact sample of B4Fr, the Na content increased compared to the samples remaining in the profile, and that no trend in K content of profile B6Mx was found.

The total amount of Fe had increased in the heater-contact samples (within 4 mm) of all materials. Bulk samples of ABM2 of all studied materials appeared to have gained CaO, and organic carbon, and lost SiO₂, MgO, Na₂O and inorganic carbon, when compared to the levels in the reference samples (Kumpulainen & Kiviranta, 2010) (Fig. 5).

Bulk mineralogy

X-ray diffraction patterns and associated *Siroquant* analysis of ABM2 samples showed that the samples of the B6Mx profile consist of smectite, illite-mica, quartz, cristobalite, plagioclase, K-feldspar, calcite, gypsum, pyrite and anatase; the samples of the B5Dep profile contain smectite, illite-mica, quartz, cristobalite, tridymite/opal, plagioclase, K-feldspar, calcite, dolomite, gypsum, pyrite and anatase and the samples of the B4Fr profile contain mixed-layer I-S, kaolinite, quartz, K-feldspar, siderite, gypsum, pyrite and anatase, with only minor deviations. In the B6Mx profile, the cristobalite content appeared to have diminished in samples closest to the heater (within 1 and 4 mm, Fig. 6, Table 1). In addition, in some samples (distances of 0–1 mm and 49–63 mm from the heater) gypsum was more pronounced compared to other samples in the profile (Fig. 6). In the B5Dep

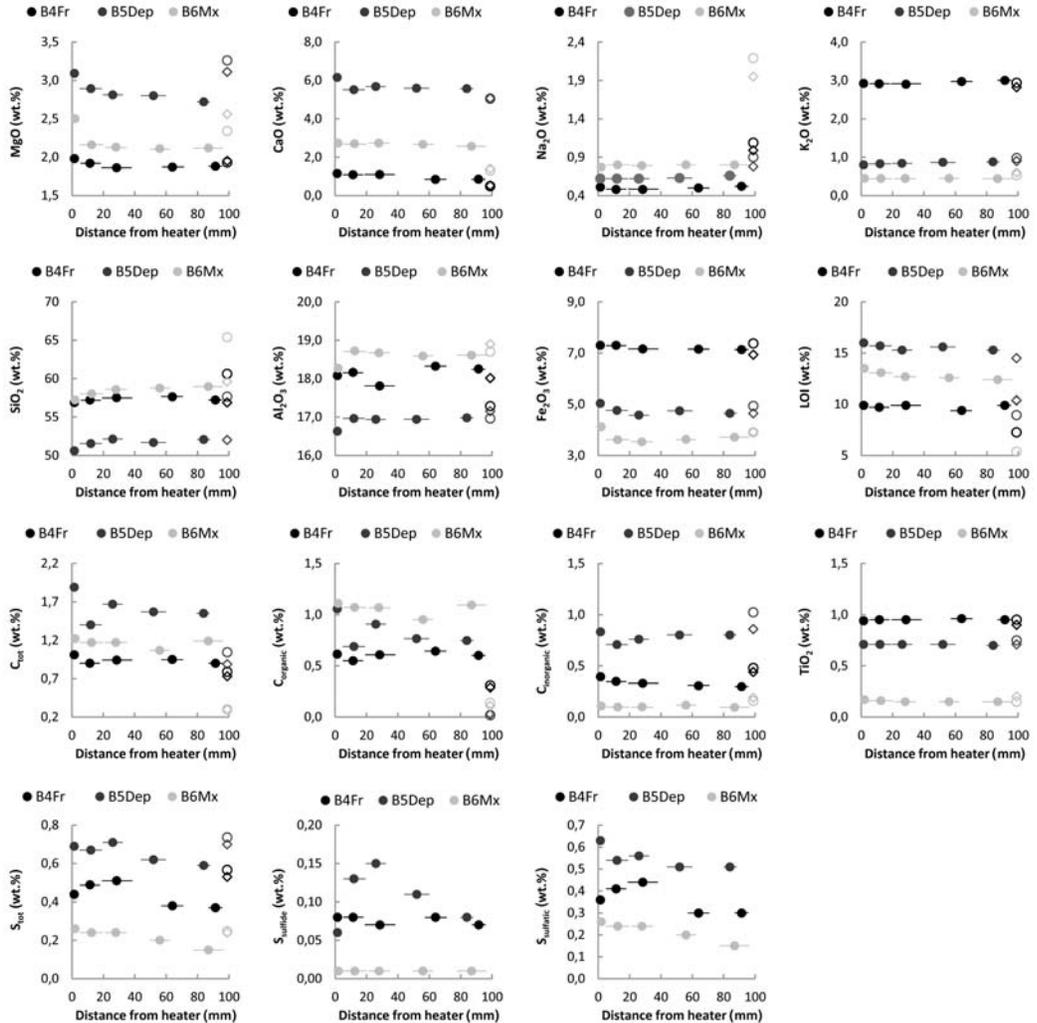


FIG. 5. Chemical compositions in horizontal profiles of the Friedland clay, Deponit CaN and MX-80 as a function of the distance from the heater. The open symbols are reference levels from Kumpulainen & Kiviranta (2010) (circles) and Svensson *et al.* (2011) (diamonds).

profile, samples taken from the zone of contact with the heater (between 1 and 3 mm) contained gypsum, and a sample within 3 mm of the heater also contained anhydrite. In the B4Fr profile, samples taken from the heater contact zone contained gypsum (Fig. 6). In samples closest to the heater (within 1 mm) there was also an indication of a decrease in feldspar contents in all materials (Fig. 6, Table 1).

Comparison of mineralogical composition results from *Siroquant* analysis (Table 1) with compositions of reference samples showed that overall there were no major changes in the bulk mineralogy.

Clay mineralogy

The positions of d_{001} reflection in bulk samples, indicative of the type of clay mineral and of the type of exchangeable cations and hydration, were approximately the same in all samples of the horizontal profiles of all materials (Fig. 6). Compared to the references, the position of the smectite d_{001} line in bulk samples, shifted from 12.6 to 14.6 Å in MX-80, from 14.3 to 14.9 Å in Deponit CaN, and from 12.7 to 14.2 Å in Friedland clay (Fig. 6).

The position of the clay minerals d_{060} reflection, which is indicative of site occupancy in the octahedral sheet and of the type of clay mineral, was the same in

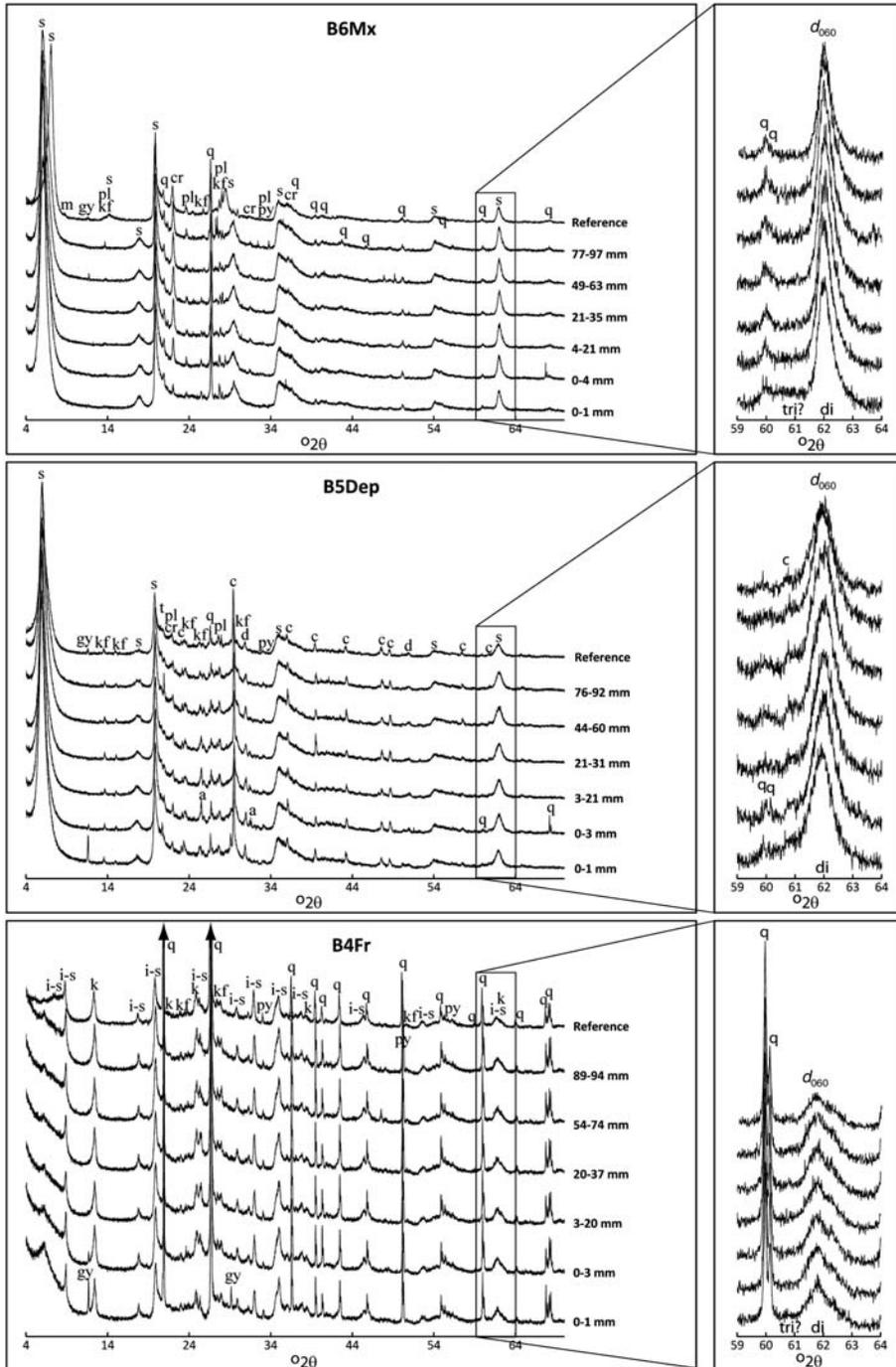


FIG. 6. XRD patterns of randomly oriented bulk samples, the minerals identified, and an enlargement of the clay minerals d_{060} region. Abbreviations: s = smectite, i-s = interstratified illite-smectite, m = illite/mica, k = kaolinite, q = quartz, pl = plagioclase, kf = K-feldspar, gy = gypsum, a = anhydrite, c = calcite, d = dolomite, cr = cristobalite, t = tridymite, py = pyrite, tri = trioctahedral, di = dioctahedral.

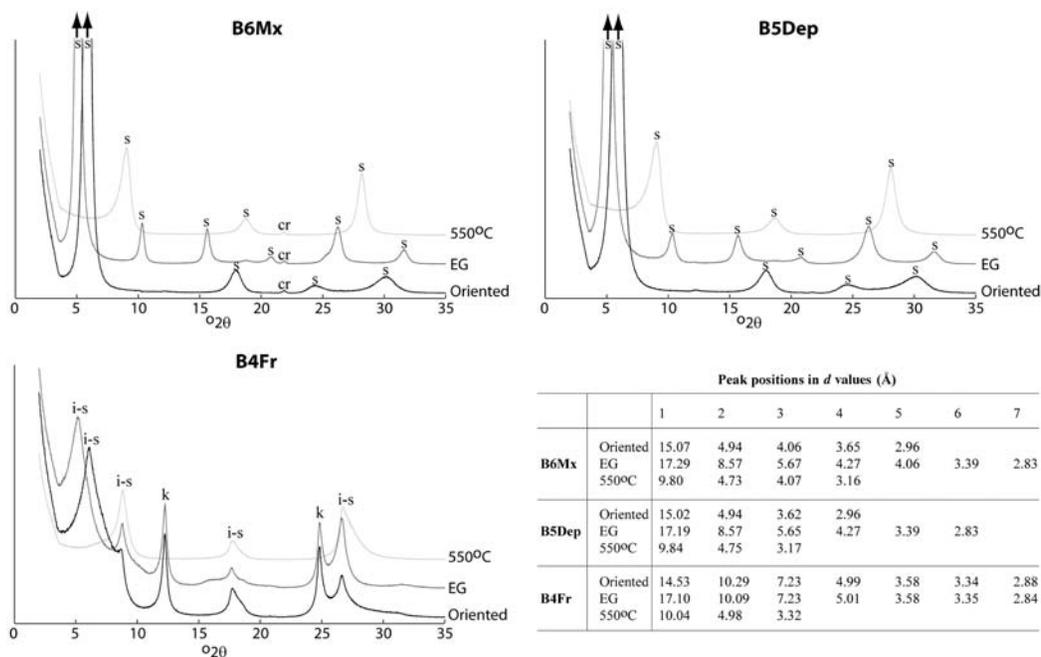


Fig. 7. XRD patterns, the minerals identified and peak positions for oriented clay fractions separated from samples at distances of 4–21 mm (B6Mx), 3–21 mm (B5Dep) and 3–20 mm (B4Fr) from the iron heater. Abbreviations: s = smectite, m = illite/mica, i-s = interstratified illite-smectite, k = kaolinite, cr = cristobalite, oriented = air dry sample, EG = ethylene glycol-solvated sample, 550°C = heat-treated sample.

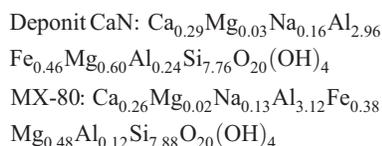
all samples of the horizontal profiles and located for MX-80 and Deponit CaN at 1.50 Å, and for Friedland clay at 1.49–1.50 Å (interstratified I-S and kaolinite). The position of the *d*₀₆₀ line was also the same as in reference samples (Fig. 6). There was a suggestion of the appearance of trioctahedral phases in samples taken 0–1 mm from the iron heater, however, as indicated by a small hump between 1.54 and 1.52 Å (60–61°2θ) in the MX-80 and Friedland clays (Fig. 6).

The purified clay fraction of MX-80 contained trace amounts of accessory cristobalite in addition to smectite; the clay fraction of Deponit CaN contained only smectite, and the clay fraction of the Friedland contained both mixed-layer I-S and abundant kaolinite (Fig. 7). All clay minerals in clay fractions were the same as in the purified clay fractions of reference samples (Kumpulainen & Kiviranta, 2010).

The CEC measurements after Li saturation and heating at 250°C showed a minor increase in the tetrahedral charge of smectite (from 23% in the reference clay fraction after Kumpulainen & Kiviranta, 2010, to 28% in clay fraction of the present study) in a sample of Deponit CaN 21–31 mm from the heater, a minor decrease in a sample of

Friedland clay 20–37 mm from the heater (from 51% in reference clay fraction after Kumpulainen & Kiviranta, 2010 to 45% in clay fraction of the present study), but no change in the sample of MX-80 21–35 mm from the heater (from 16% in the reference clay fraction after Kumpulainen & Kiviranta, 2010, to 15% in the clay fraction in the present study).

The structural formulae of smectites calculated from the chemical compositions of the purified <0.5 μm clay fractions, CBD extractions and initial exchangeable cation compositions (Fig. 1c) determined from samples ~3–21 mm from the heater were as follows:



The beidellite contents calculated from structural formulae were 30% for Deponit CaN and 17% for MX-80, comparable with the results from a quantitative Greene-Kelly test: 28% and 15%, respectively.

Because the chemical compositions and XRD analyses were made on the same <0.5 μm batch, and

the only identified source of error in the calculation of the smectite structural formulae was the tiny amount of SiO₂ polymorphs in the sample of MX-80, appearing as a tiny hump at *d* spacing = 4.04 Å. Comparison of smectite structural compositions of MX-80 and Deponit CaN from ABM2 with structural compositions of smectites of similar origin (Kiviranta & Kumpulainen, 2011) showed a small increase in tetrahedral charge (increase in tetrahedral Al content from 0.05 moles to 0.12 moles and from 0.10 moles to 0.24 moles, respectively), but no change in total charge. These changes are rather small and are considered to be within the precision of the method.

Calculated CEC values for smectites of ABM2 samples were in line with the measured CEC values of the clay fraction for samples from B6Mx (0.92 eq/kg and 0.95 eq/kg, respectively) and B5Dep (1.06 eq/kg and 1.03 eq/kg, respectively).

Hydromechanical tests

Core-drilled samples of Friedland clay in ABM2 showed a ~0.5–2 MPa decrease in a swelling pressure (Fig. 8) compared to the reference samples (Kumpulainen & Kiviranta, 2011). The decrease was larger for samples taken closer to the heater. After grinding and recompaction of samples, however, the swelling pressure was recovered. For the Deponit CaN and MX-80 samples, the swelling pressure did not decrease, at least by not more than in the ABM1 samples (Kumpulainen & Kiviranta 2011; Svensson *et al.*, 2011). No changes in hydraulic conductivities were observed in any of the samples tested.

DISCUSSION

Groundwater–bentonite interaction

The major changes in exchangeable cations as well as in Na, K, Ca and Mg total contents compared to reference samples might originate from interactions, namely saturation and cation exchange, with Äspö groundwater. In general, the changes in exchangeable cation populations in ABM2 samples were clearly more pronounced than observed previously (Kumpulainen & Kiviranta, 2011; Dohrmann *et al.*, 2013). Dohrmann *et al.* (2013) found that the exchangeable cation compositions in ABM parcel 1 varied considerably between the blocks, and that blocks located in the upper part of the parcel were richer in Ca than blocks located in the bottom part of the parcel. Those authors also noted that the influence

of neighbouring blocks on cation compositions was much less important than the position within the test parcel. Similar variation in exchangeable cation compositions between different blocks of material was not observed in the present study probably because the blocks selected were located side by side, and because the equilibration time was longer (6.5 y in ABM2 vs. 2.5 y in ABM1).

In ABM2, the exchangeable cation population in Friedland clay (27–33% Na, 3–4% K, 5–6% Mg and 58–64% Ca) differed slightly from MX-80 and Deponit CaN (19–22% Na, 0–1% K, 5–7% Mg and 71–75% Ca), resulting either from lack of equilibrium in exchangeable cation reactions, or from differences in the affinity of exchangeable cations towards mineral surfaces between different materials. The latter explanation is considered more probable because the mineralogical composition of Friedland clay is rather different from those of Deponit CaN and MX-80.

Fe–bentonite interaction

Iron in the heater influenced the clays studied very locally. The total amount of iron did not increase in the B6Mx, B5Dep, or B4Fr profiles in the ABM2 experiment, except for some minor accumulation in the B6Mx and B5Dep profiles directly at the contact with the iron heater, within 3 mm. A decrease in CBD-extractable Fe appears in the horizontal profiles of Deponit CaN and Friedland clay towards the steel heater, however. Furthermore, the amount of CBD-extractable Fe was smaller in ABM2 Deponit CaN and Friedland clay samples than in the reference samples or in ABM1 samples (Kumpulainen & Kiviranta, 2011). Thus, Fe previously bound in poorly crystalline Fe oxides was reduced, the crystallinity of Fe oxides might have improved due to thermal effects, or the Fe phases were altered (*e.g.* precipitation of maghemite or magnetite both of which are less soluble in CBD). Such changes are thought to result not from Fe–bentonite interaction, but rather from other reactions, *e.g.* from thermal effects. Neoformed Fe-bearing mineral phases and increase in existing Fe-bearing mineral phases, or changes in the smectite compositions (in terms of Fe content) were not observed. As the sampling and sample preparations were performed in oxidative conditions, conclusions on Fe speciation could not be given. Furthermore, as the sampling was restricted by the amount of material needed for the analyses, mineralogical changes may have occurred at the contact (see Svensson, 2015, for example) but could

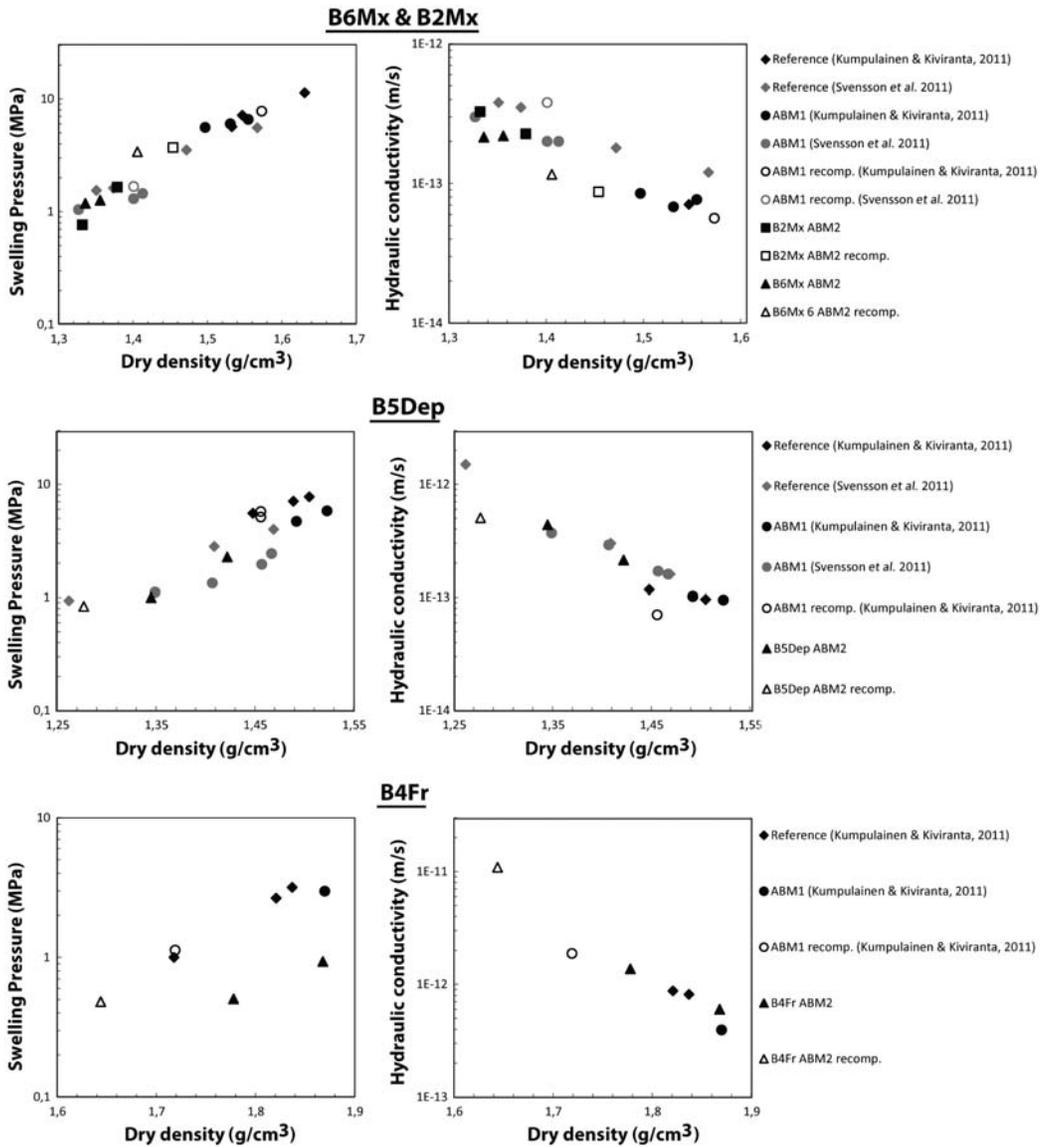


FIG. 8. Swelling pressure and hydraulic conductivity of drill-cored samples (filled symbols) and recompacted samples (open symbols) from the present study (ABM2) as a function of dry density. Reference samples (diamonds) and samples from previous studies (ABM1, circles) are shown for comparison with results in the present study (ABM2).

not be detected in the present study due to dilution effects.

Alteration of the clay materials due to thermal effects

Elevated temperature and prevailing temperature gradients were important reasons for many of the

changes observed. Overall, the observed changes in ABM2 were similar to those seen in other long-term *in situ* heating tests such as LOT (Karnland *et al.*, 2009), TBT (Åkesson *et al.*, 2012) or Prototype (Olsson *et al.*, 2013; Dohrmann & Kaufhold, 2014).

Water extractions showed that sulfate salts had accumulated at the heater contact (Deponit CaN and MX-80) or at distances of 4–35 mm from the heater

(Friedland clay). Salts consisted mostly of Ca and SO₄, but small amounts of Mg and K were assumed to have coprecipitated with CaSO₄. The amounts of water-soluble Cl in Deponit CaN, Friedland clay, and MX-80 in ABM2 test were greater than those observed by Muurinen (2010) and Svensson *et al.* (2011) from the ABM1 experiment, but the amounts of water-soluble SO₄ in these materials of the ABM2 test were generally smaller than observed in the ABM1 test by Muurinen (2010) and Svensson *et al.* (2011). Thus, soluble salts were considered to have been redistributed within the blocks rather than accumulated towards the heater with time.

The sum of exchangeable cations was less than the CEC measured in MX-80 and Deponit CaN. The apparent decrease in the sum of exchangeable cations did not result from the decrease in CEC because the CEC was the same as the reference values. The discrepancy in the sum of exchangeable cations and CEC is probably related to methodological uncertainty in exchangeable cation extraction of calcareous and/or gypsiferous bentonites (MX-80 and Deponit CaN) as discussed previously (Dohrmann & Kaufhold, 2010; Dohrmann *et al.*, 2012b).

The observed decrease in CBD-extractable Fe as a function of distance from the heater in Deponit CaN and Friedland clay could be explained by improvement in crystal order of Fe phases due to thermal effects.

Both this and previous studies (Svensson *et al.*, 2011; Olsson *et al.*, 2013) have shown that Mg was accumulated towards the heater. Interestingly, in this study, not only total and water-soluble Mg, but also CBD-extractable Mg appeared to have accumulated towards the heater. It was assumed that CBD extraction was capable of dissolving Mg-containing newly formed phases, *e.g.* Mg-hydroxides or Mg-sulfates. Note, however, that when compared to reference levels, the CBD-extractable Mg decreased significantly.

Mineralogical analysis indicated the accumulation of gypsum and dissolution of cristobalite, tridymite/opal and feldspars near the heater. Such changes are generally in line with the chemical data. Dissolution of cristobalite has been observed in the ABM1 samples close to the Fe heater (Kaufhold *et al.*, 2013). The reason for dissolution of cristobalite, but also of tridymite/opal and feldspars in this study might be related to elevated porewater pH that originated from corrosion of Fe (Dohrmann & Kaufhold, 2014).

The comparison of chemical composition-based calculated mineralogical compositions (values in parenthesis in Table 1) with mineral contents gained from mineralogical analysis showed that the pyrite

content was overestimated, and gypsum contents were underestimated in all materials. Moreover, the calcite contents were overestimated for MX-80. The reason for the discrepancy was assumed to result from uncertainties in both mineralogical and chemical analyses. For example, accessory mineral contents were close to the detection limit of XRD (~1 wt.%).

The appearance of a weak d_{060} hump in the XRD patterns of clay minerals suggested that trioctahedral clay minerals might have been formed in samples in contact with the iron heater. Samples from ABM2 block 9 (Febex), much closer to the heater than the samples in the present study were analysed by Svensson (2015) who found more robust XRD evidence for the existence of trioctahedral clay minerals as well as supporting chemical and FTIR data which suggested the presence of Fe-saponite.

The reason for increased organic carbon content could not be explained. The source was probably not the lubricant used for compressing the blocks, because organic-carbon content increased uniformly in all ABM2 samples, not just at block edges (which showed elevated Mo and Zn contents and these do indicate an influence by the lubricant). Furthermore, the possibility of analytical error was also excluded as the control samples analysed at the same time showed no evidence of excess organic carbon. Thus, the increase in organic carbon content was thought to have resulted from artefact, *i.e.* contamination of samples during storage, in spite of keeping them vacuum packed during storage.

The observed decrease in swelling pressure of core-drilled samples of Friedland clay that was recovered after grinding and recompaction was in line with previous studies (Kumpulainen & Kiviranta, 2011; Svensson *et al.*, 2011). Note also that the swelling pressure of core-drilled samples of MX-80 and Deponit CaN did not decrease – at least by no more than observed previously in the ABM1 experiment (Kumpulainen & Kiviranta, 2011; Svensson *et al.*, 2011).

CONCLUSIONS

The chemical and mineralogical effects observed in the ABM2 test were more pronounced than those in the ABM1 test probably due to the longer duration of the test (5 y of heating in the ABM2 test compared to 2.5 y in the ABM1 test). In ABM2, three types of chemical effects were recorded: uniform changes occurred in blocks, rising or falling trends in horizontal profiles of

the blocks, and changes occurring only at the boundary with the iron heater.

Changes occurring uniformly in blocks might result from interactions with the Äspö groundwater, rising or falling trends in horizontal profiles might originate from thermal interactions, and changes at the boundary with the iron heater might result either from interactions with the iron heater or because of thermal effects.

Compared to the reference samples, the exchangeable cation populations changed uniformly in all blocks. Increases in water-soluble Ca, Mg, K and SO₄, decreases in poorly crystalline Fe oxides, increase in the total amounts of Mg, Ca, S and decreases in the total amounts of Na and K were noted in horizontal profiles towards the heater. At the boundary with the heater, increase in Fe and decreases in the amounts of Si and Al, the precipitation of gypsum and anhydrite, indications of the formation of trioctahedral clay minerals, and the dissolution of cristobalite and feldspars were observed. In addition, a decrease in the swelling pressure of core-drilled samples of Friedland clay was observed that was recovered after grinding and recompaction. No change in hydraulic conductivity was observed in any of the materials studied.

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