

## EBSD Analysis Optimised for Twin-related Boundaries

Valerie Randle

Dept. Materials Engineering, University of Wales Swansea, Swansea SA2 8PP, UK.

The nickel-based superalloy Nimonic PE16 is precipitation strengthened by the presence of gamma-prime. Overaging the alloy results in an increase in the pinning force on the boundary of at least a factor of two, and the grain size is very stable when the alloy is annealed below the gamma-prime solvus, namely 880°C [1,2]. Another microstructural feature of PE16 is that annealing twins are readily formed because of its low stacking-fault energy. Experiments have been conducted to explore the evolution of grain boundary parameters in PE16. Specimens of commercially heat treated PE16 were annealed in air at 850°C, i.e. 30°C below the gamma-prime solvus, for times of 1h, 10h and 100h. Misorientation data across interfaces were obtained by use of an electron back-scatter diffraction (EBSD) system from HKL Technology in a Philips XL30 SEM [3]. Several orientation maps with a grid step size of 0.5µm were collected and analysed from each specimen.

Figure 1 shows a typical example of an orientation map from overaged PE16. In the coincidence site lattice (CSL) system boundaries are categorised by  $\Sigma$ , the reciprocal density of coinciding sites. In figure 1  $\Sigma 3$  boundaries are represented as thick white lines,  $\Sigma 9$  and  $\Sigma 27$  boundaries are thin white lines and other boundaries are black. The statistics for the  $\Sigma 3^n$  family are shown in figure 2. Apart from  $\Sigma 3$ , plus some  $\Sigma 9$  and  $\Sigma 27$ , there were almost no other  $\Sigma$  boundaries recorded. There was a small increase in  $\Sigma 3$  proportion from 43% after 1h annealing to 50% after 100h. More than 90% of the total length of  $\Sigma 3$  in the map is within 2° of the exact reference misorientation, which indicates that these  $\Sigma 3$ s are predominantly annealing twins. The remaining 10% of  $\Sigma 3$  length deviates by more than 2° from the reference structure. It is evident from the morphology of these higher deviation  $\Sigma 3$ s that they are more akin to grain boundaries than to twins.

Higher  $\Sigma 3^n$  boundaries in the microstructure are usually generated by impingement of two appropriate  $\Sigma 3^n$  boundaries, e.g.  $\Sigma 3 + \Sigma 3 \rightarrow 9$ ,  $\Sigma 3 + \Sigma 9 \rightarrow 27$ . The proportions of  $\Sigma 9$  and  $\Sigma 27$  in the present data are particularly low, which is an indication that there has been little movement and interaction of  $\Sigma 3$ s, hence disallowing their impingement. This also explains why most  $\Sigma 3$ s are twins: there has been very little impingement to produce  $\Sigma 3$ s via 'back' reactions of the type  $\Sigma 9 + \Sigma 3 \rightarrow \Sigma 3$ , which is expounded in the 'Σ3 regeneration model' [4]. This near-stagnation in the grain boundary population is a result of the strong grain boundary pinning by gamma-prime precipitates which inhibited grain boundary migration.

### References

- [1] W. Betteridge and J. Heslop, *The Nimonic Alloys*, Edward Arnold, London, 1974.
- [2] V. Randle and B. Ralph, *Acta Metall.* 34 (1986) 891.
- [3] V. Randle and O. Engler, *Introduction to Texture Analysis: Macrotecture, Microtexture and Orientation Mapping*, Gordon and Breach, London, 2000.
- [4] V. Randle, *Acta Mater.* 47 (1999) 4187.

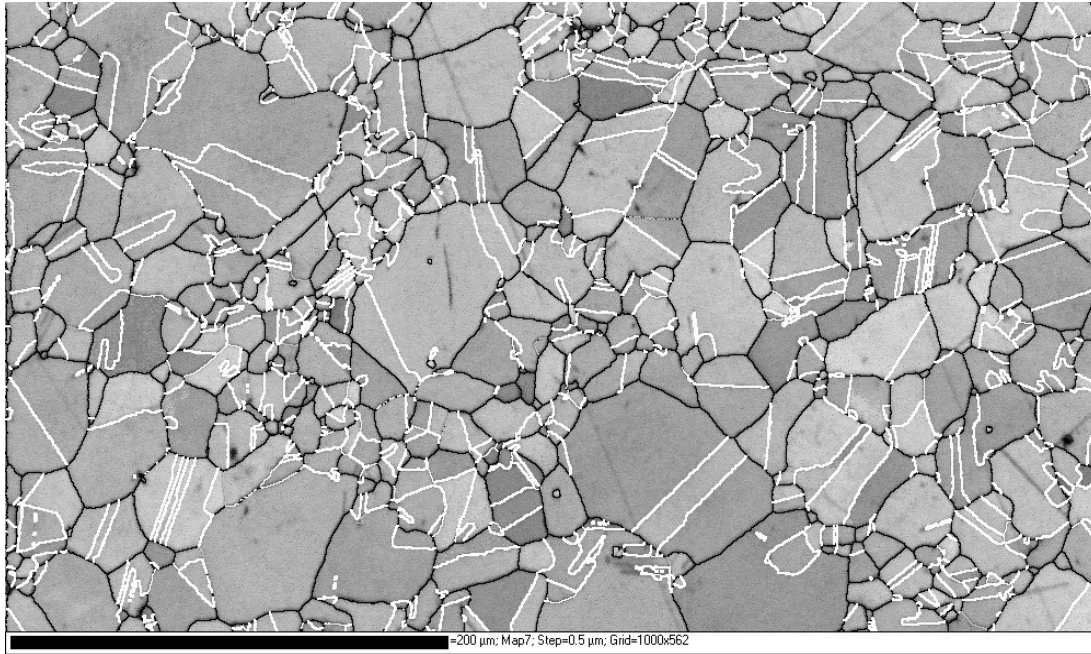


Figure 1. Example of an orientation map from PE16 after annealing for 10h.  $\Sigma 3$  boundaries are represented as thick white lines,  $\Sigma 9$  and  $\Sigma 27$  boundaries are thin white lines and other boundaries are black.

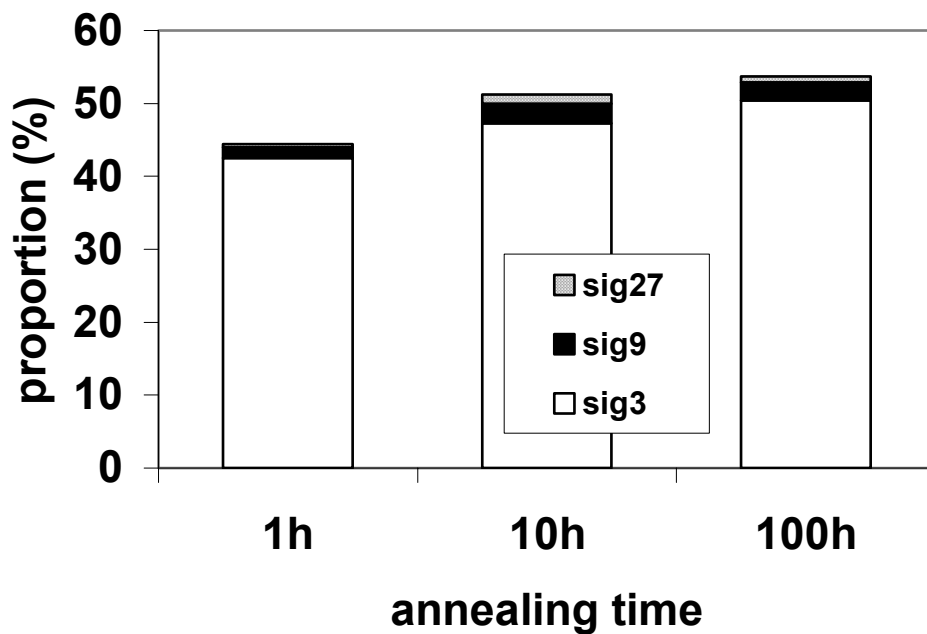


Figure 2. Proportions of  $\Sigma 3^n$  boundaries after 1h, 10h and 100h annealing below the gamma-prime solvus. The scale bar is 100 $\mu\text{m}$ .