

## Effect of Ni Addition and T6 Heat Treatment on Microstructure and Microhardness of Hot Plastic Deformed (Al-Si-Mg) Alloys

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A356 (Al-Si-Mg) alloy have been widely used in the automotive, aerospace and military industries due to their high castability, corrosion resistance and excellent strength/weight ratio. The most important alloying elements are Si and Mg. The microstructure of A356 alloy in as-cast condition is composed mainly by Al- $\alpha$  dendrites, interdendritic Al-Si, Mg<sub>2</sub>Si phase and Fe-based intermetallics. The main applications are in the automotive, aerospace and military industries. Excellent mechanical properties of A356 alloy are obtained after T6 heat treatment, because to precipitation of  $\beta''$ -Mg<sub>2</sub>Si and  $\beta'$ -Mg<sub>2</sub>Si coherent and semi-coherent metastable phases. In recent years previous researches have reported that an excellent combination of strength and ductility can be achieved by adding alloy elements, as well as, performing heat treatments and deformation processes. An example of such elements to reinforce Al Alloys are transition elements (Ni, Fe, Zr, Ti and V), these elements have been used due its low solubility in Al (0.01 % to 0.03 %) and high ability to form intermetallic compounds. It has been reported that additions of 1 to 2 Ni (wt. %) to Al alloys of the series 3xxx and 2xxx increase the hardness and tensile/wear properties because of to the formation of Al-Ni and Al-Ni-Cu intermetallic compounds, allowing that these alloys can be used in applications at relative high temperatures [1-5]. Thus, this investigation is focused to the variations on microstructure and hardness generated by Ni additions, hot plastic deformation and T6 heat treatments in A356 alloy.

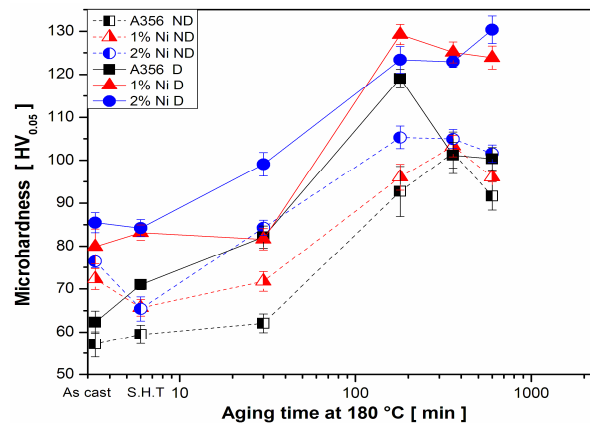
A356 alloy and those modified with Ni (1-2 wt. %) were hot plastic deformed at 350 °C with 50% deformation ratio, solution heat treated (SHT) at 535 °C for 7 h, quenching in water at 60 °C and aged at 180 °C for different period of time. Changes in the microstructure and hardness were characterized and evaluated by TEM HITACHI 7700 (operated at 120 kV) and Jeol JEM2200F+CS (operated at 200 kV) and Vickers microhardness was evaluated in LECO LM300 AT tester.

The Fig. 1 shows the behavior of the microhardness values respect to Ni content, hot-plastic-deformation (D) or non-deformation (ND) and aging time in A356 alloy. There are observed increments of hardness values as a function of Ni concentration. The hardness peaks are observed at 180 min (3 h) for (ND) and 600 min (10 h) for (D) alloys both with 2 Ni (wt. %). The graph illustrates similar behavior for both (D) and (ND) with 1-2 Ni (wt. %) alloys, the hardness values remain stable since 3 h to 10 h. The Ni additions and hot plastic deformation in A356 alloy favors the increments in HV values. Additionally, in samples alloyed with Ni the HV values decreases slowly during over-aging stage. Furthermore, the Ni addition 1-2 Ni (wt. %) to the A356 alloy have an important effect on the

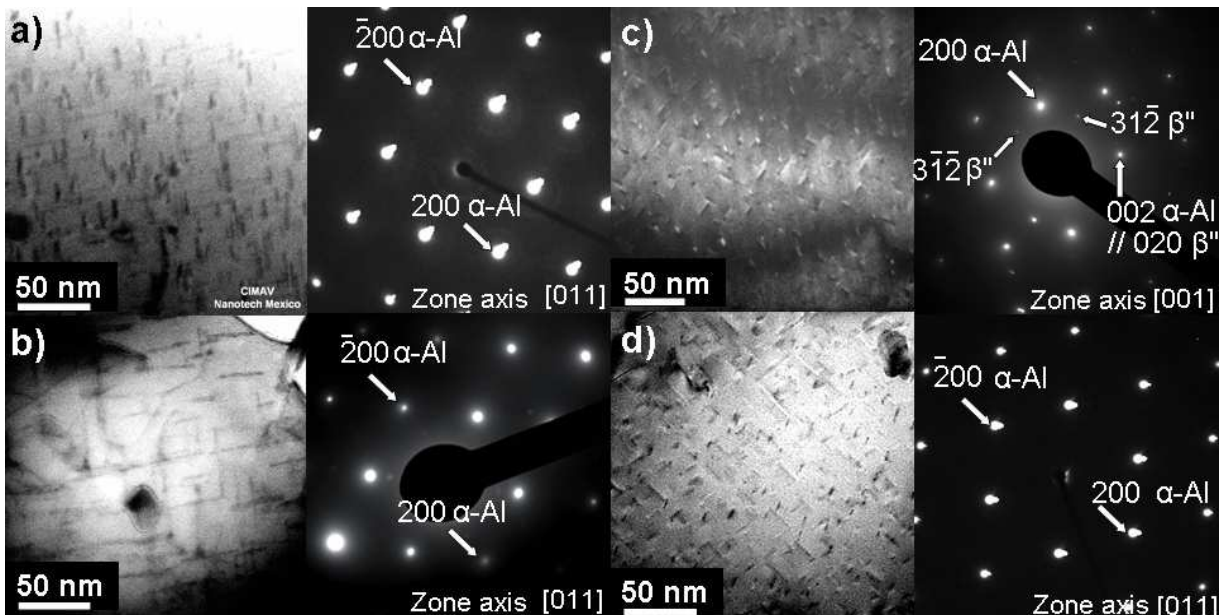
microstructure; mainly in the morphology, size, distribution and number density of  $\beta$ - $Mg_2Si$  precipitates formed during aging heat treatment (Fig. 2).

#### References:

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**Figure 1.** Evolution in hardness values respect to Ni content, hot-plastic-deformation (D) or hot-plastic-non-deformation (ND), and aging time after 7 h of solution treatment.



**Figure 2.** TEM Micrographs and SAD patterns of deformed and T6 heat treated alloys. a) and b) Bright field (BF) micrographs of reference alloy aged for 3 and 10 h respectively, c) and d) dark field (DF) and (BF) micrographs of A356 alloys alloyed with Ni aged for 3 and 10 h respectively.